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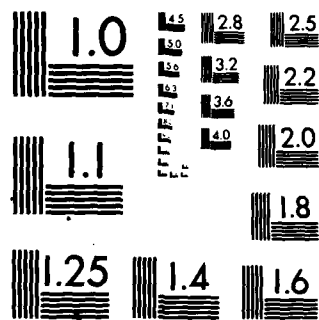
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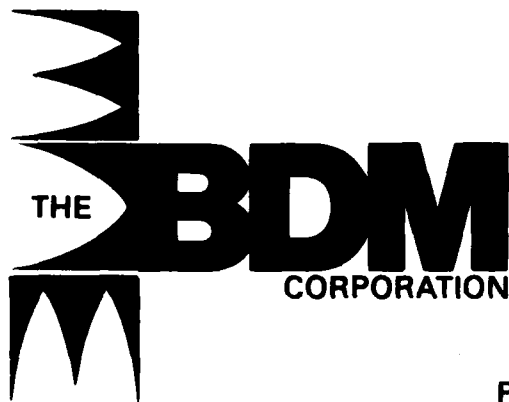
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STREX  
A PRELIMINARY REPORT OF  
NAVAL POSTGRADUATE SCHOOL DATA

by  
DONALD E. SPIEL  
Project Engineer

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## FOREWORD

This report was prepared under Work Order No. 315 of Contract No. N00014-79-C-0088 in support of the U.S. Naval Postgraduate School research project supported by the Naval Air Systems Command, AIR370, and the Naval Program Office, EO/MET. The report was produced at the request of Professors K. L. Davidson and G. E. Schacher.

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## ABSTRACT

A preliminary report on the data gathered by the Environmental Physics Group of the Naval Postgraduate School during the Storm Transfer and Response Experiment (STREX) is given. All meteorological measurements made during the experiment along with some of the parameters derived from these measurements, e.g.,  $Z/L$ ,  $U_*$  and  $U_*\epsilon$ , are listed. The times of radio interference have been determined and tabulated. Data anomalies have been noted. No aerosol results are given.

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## A. INTRODUCTION

The Environmental Physics Group of the Naval Postgraduate School (NPS) participated with other scientific groups in a study of oceanographic and meteorological factors influencing and influenced by the passage of storm fronts. This effort, known as the Storm Transfer and Response Experiment (STREX), took place in the Gulf of Alaska in November and December of 1980 on board the NOAA Ship Oceanographer. It was the responsibility of NPS to provide measurements of aerosol spectra and certain other meteorological parameters important to an understanding of the surface generation and flux of aerosols, and the turbulent transport of heat, humidity and momentum.

This is a preliminary report of the NPS data. That this is a preliminary report should be emphasized. Until the effect of such factors as radio interference and the variation of certain parameters with the relative wind direction, to name only two, are finally determined, the data should be treated with caution.

## B. INSTRUMENTATION

### 1. The quantities measured by NPS during STREX were:

- 1) Sea surface temperature,  $T_s$
- 2) Infrared sea surface temperature,  $T_{ir}$
- 3) Air temperature,  $T_a$
- 4) Dew point temperature,  $T_d$
- 5) Relative Humidity, RH
- 6) Relative wind speed,  $U_r$
- 7) Wind speed fluctuations,  $V_{rms}$
- 8) Inversion height (if less than ~ 700 meters)
- 9) Aerosol spectrum from 0.25 to 12.5 microns radius (Instruments were on board to measure the spectrum from .08 to 152 microns, but equipment failures narrowed the range.)

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In addition, analog signals for ship's speed, heading and the relative wind direction were provided by the ship and monitored as needed.

Table I lists the instrumentation used by NPS during STREX. Since this equipment has been described elsewhere <sup>1/</sup>, only a brief description will be given here.

A single computer was used to direct the accumulation of both the meteorological and aerosol data. Appendix A contains a printout of this program along with a description of the matrices, special function keys and strings output to the data files.

Data for both aerosols and meteorology were accumulated for 30 minute periods and output to the printer and cassette tape as averages over this period. In addition, the aerosol data and some of the meteorological data, see Table II, were recorded by the Kennedy in 20 second averages. The meteorological data were passed to the Kennedy by way of the PMS housekeeping modules which calculated the averages. It was necessary, early in the cruise, to remove the ship's analog signals for ship's speed and heading and relative wind direction from the input to the PMS. The source of these signals was of such a high impedance that, even though the input impedance of the PMS housekeeping modules was also large, the modules loaded the source and thereby introduced errors. These signals therefore are either not on the Kennedy tape or are inaccurate when they are.

The sensors for wind speed, relative humidity, air temperature, dew point and wind speed fluctuations were mounted on the foremast, 28 meters from the waterline. The aerosol probes were also mounted on the foremast, 22 meters from the waterline. These locations were chosen to minimize the influence of the ship on the measurements. The sea surface probe entered the water from a 12 foot boom located on the starboard side of the ship just aft of the bridge. The ship's engine cooling water exhausts were on the port side. The IR radiometer was on the starboard side near the bridge

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TABLE I. EQUIPMENT USED DURING STREX

Hewlett-Packard (HP) Computer Model 9825S  
HP Scanner Model 3495A  
HP Relay Actuator Model 59306A  
HP Digital Clock Model 59309A  
HP Digital Voltmeter Model 3455A  
Particle Measuring Systems (PMS) Data Acquisition System Model DAS-64  
PMS Probe Model ASASP-500  
PMS Probe Model CSASP-100-HV  
PMS Probe Model OAP-230X  
Kennedy Incremental Tape Recorder Model 1600/360  
General Eastern Dewpoint Hygrometer Model 1200AP  
Thermo-Systems (TSI) Constant Temperature Anemometer Model 1054B  
TSI Probe Model 1200 with Sensor Model 60  
Aerovironment Acoustic Radar Model 300  
Hygrodynamics Relative Humidity-Temperature Indicator Model 15-3057  
Nicolet Scientific Spectrum Analyzer Model 440B  
Barnes Engineering Radiation Thermometer Model PRT-5  
Meteorology Research, Inc. Transmuter Model 1001 and Sensor Model 1022  
Krohn-Hite Band Pass Filter Model 3750  
Rosemount Platinum Resistance Thermometer Series 78 (three each)  
HP Strip Chart Recorder Model 7132A (two each)  
HP Printer Model 9871A

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TABLE II. INPUTS TO THE KENNEDY VIA PMS  
ANALOG HOUSEKEEPING MODULES

Input No.	Function
A2	PMS Active Scattering Probe Laser Output
A3	Relative Wind Speed
A4	Relative Wind Direction
A5	Ship's Heading
A6	Ship's Speed
A7	Average Hot Film Voltage
A8	Air Temperature (from Hygrodynamics Digital II)
A9	Relative Humidity
B2	PMS Classical Scattering Probe Laser Output
B3	Barnes IR Sea Surface Temperature (NPS)
B4	Barnes IR Sea Surface Temperature (U of W)
B5	Hot Film $V_{rms}$ Voltage

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and oriented to view the sea just beyond the ship's wake ( $\sim 35^\circ$  with respect to the horizontal). The acoustic sounder was on the fantail just forward of the crane. All other equipment was located in the plotting room just aft of the bridge, at the base of the foremast.

### 2. Major equipment failures during STREX were as follows:

1) Wind fluctuations probe: There were a total of four probes, three for back-up, mounted side by side. Only one of these was ever in use and it failed at 1230 hours on 17 November. All three back-ups, which were not kept hot, had failed at some unknown time prior to this. It was not possible to safely replace these probes while the ship was at sea, so they were not replaced until the Ketchikan layover between Legs I and II of STREX. One of the replacement probes did not survive its mounting. During Leg II all three remaining probes were heated continuously and only one, a back-up, failed.

2) The IR radiometer failed prior to the beginning of Leg I, due to water incursion, but was repaired and placed in operation at 2200 hours on 11 November. During Leg II the indicated temperature gradually increased until it became apparent that the measurement could not be correct. Subsequent to STREX it was found that the radiometer lens was covered by a nearly opaque layer of sea salt.

3) Aerosol probes: neither the ASASP nor the OAP aerosol probes functioned during any of STREX. Later it was found that both probes had been inundated with water and that the OAP had suffered serious physical damage (probably during the very rough night of November 4-5).

4) Relative Humidity: the relative humidities reported below were calculated from the dew point measurements. There was on board, however, a Hygrodynamics humidimeter used as a back-up. It did not function during any of Leg I because of a broken lead in a cable and functioned only intermittently during Leg II for reasons not yet known. It provided no useful data for any of STREX.

5) Ship's Analogs: the ship's analog outputs for ship's speed and heading and relative wind direction were incorrect from the start of

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Leg I until about 1100 hours on 7 November. This condition prevailed not only because the outputs were loaded, by others as well as NPS, but also because they were incorrectly calibrated.

Radio transmissions from the ship had a profound effect on some of the measurements. Most seriously affected were the wind fluctuations, sea surface temperature and IR radiometry. The latter measurement, which was recorded continuously by a strip chart recorder, was such an infallible indicator of RFI that it was used to plot the periods of interference.

Wind fluctuations  $V_{rms}$  and relative wind direction were also recorded continuously by a strip chart recorder.

### C. PRELIMINARY DATA

A summary of the meteorological data and some of the quantities derived from them is given in Appendix B. The temperatures  $T_a$ ,  $T_s$  and  $T_d$  have been corrected for erroneous calibration constants utilized during STREX and a guestimated correction has been applied to those quantities affected by the incorrect ship's analogs. The latter applies only to the first 60 files of data tape number 1. An absence of data indicates instrument failure. The calculations of  $Z/L^{2/}$ ,  $U_{*}^{3/}$  and  $U_{*}\epsilon^{4/}$  are described elsewhere.

The sea surface thermometer was removed from the sea by the crew, on several occasions, during buoy recovery operations. This happened on November 17 affecting  $T_s$  for File 154 of Data Tape 2 (the cable was accidentally severed at that time), and again on November 21 during the accumulation of data for File 64 of Data Tape 3. There may have been other occasions of thermometer removal of which we were not aware.

The acoustic radar, which ran and recorded continuously, detected an inversion only in the period 1900 hours, December 7, to 0400 hours, December 9, during which the height of the inversion varied between 200 and 400 meters.

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A list of times of probable radio interference is contained in Appendix C. These times were extracted from the IR strip chart for the period when the radiometer was functioning (2200 hours November 11 through 2345 hours December 12) and otherwise from the  $V_{rms}$  strip chart. The RFI record on the  $V_{rms}$  chart is confused by other factors which may cause anomalous readings. Periods of RFI can be detected on the  $V_{rms}$  record only when the other factors are not affecting  $V_{rms}$ . The list of probable RFI times is, therefore, not complete for those periods when the radiometer was not operating. A compilation of data files probably affected by RFI is also given in Appendix C.

The location of the hot film relative to other sensors and to the ship's structure was such that relative winds within  $\pm 60^\circ$  of the bow should have yielded valid values of  $V_{rms}$ . There were periods, however, when, with relative winds within this arc, and with no RFI,  $V_{rms}$  was anomalously large. The times of these anomalies is tabulated in Appendix D. A list of affected files is included there.

For reasons not yet understood, winds from the port quarter at angles of  $345^\circ$  and below gave rise to excessive  $V_{rms}$ . At times winds from the starboard quarter within  $30^\circ$  of the bow also yielded large  $V_{rms}$ , but these could be correlated with the occasional fouling of the tether which was used to constrain the rotation of the hot film holder.

In the meteorological data summary of Appendix B the notation at the ends of rows denotes which files were affected by RFI and/or anomalous  $V_{rms}$  and for how long. For example, an R20 following a row of data denotes 20 minutes of RFI during the averaging period and a V13, say, would signify that although the average relative wind direction was within a  $\pm 60^\circ$  arc of the bow, there was 13 minutes of anomalously large  $V_{rms}$ . An asterisk is used to denote those files for which the average relative wind direction was greater than  $60^\circ$  but less than  $300^\circ$ .

No summary of the aerosol data is given in this report. The failure of ASASP probe will preclude, in future analysis, the separation of the continental component from the aerosol spectrums measured during STREX. The failure of the OAP probe means that the hoped for extension of our knowledge of aerosols to larger radii did not occur during STREX.



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## APPENDIX A

### STREX COMBINED AEROSOL AND MET DATA ACQUISITION PROGRAM

#### I. List of Matrices and their content

P[I,J] Raw MET Voltages  
 U[I,J] Calculated MET Parameters  
 K[I,J] Permanent Scanner Channel Assignments  
 L[I,J] Temporary Scanner Channel Assignments

For these matrices I goes from 1 to 3 and J from 1 to 5 and correspond to the following quantities:

J	I = 1	I = 2	I = 3	
1	Relative Wind Speed	$T_a$ (HYGRO)	$T_d$	
2	Relative Wind Direction	RH (HYGRO)	$T_a$ (Pt)	
3	Ship's Heading	IR (NPS)	$T_s$	
4	Ship's Speed	IR (U of W)	$\left\{ \begin{array}{l} \text{True Wind Speed} \\ \text{True Wind Direction} \end{array} \right\}$	For U[I,J] Only
5	Hot Film <V>	Hot Film $V_{rms}$		

Method of Calculation (where required) for U[I,J] from P[I,J]:

J	I = 1	I = 2	I = 3
1	$10P[1,1]$	$P[2,1]$	$(P[3,1]-D[1])/ \alpha_1 D[1]$
2	$72P[1,2]$	$P[2,2]$	$(P[3,2]-D[2])/ \alpha_2 D[2]$
3	$72P[1,3]$	$10(P[2,3]-1)$	$(P[3,3]-D[3])/ \alpha_3 D[3]$
4	$8P[1,4]$	$10(P[2,4]-1)$	
5	$P[1,5]$	$P[2,5]$	

Where the  $D[*]$  are the  $0^\circ\text{C}$  resistances of the Pt thermometers and have the following correspondence:

$D[1]$   $T_d$   
 $D[2]$   $T_a$   
 $D[3]$   $T_s$

The  $\alpha_i$  are the temperature coefficients of resistivity.

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The value of these constants used during STREX were:

$$\begin{array}{ll} D[1] = 99.5989 \, \Omega & \alpha_1 = .003842 \, \Omega/\Omega/^\circ\text{C} \\ D[2] = 99.4823 & \alpha_2 = .00385 \\ D[2] = 99.4433 & \alpha_3 = .00385 \end{array}$$

Subsequent to STREX it was discovered that some of these values were incorrect. The corrected values (used for all calculations subsequent to STREX) are:

$$\begin{array}{ll} D[1] = 100.300 \, \Omega & \alpha_1 = .003942 \, \Omega/\Omega/^\circ\text{C} \\ D[2] = 100.100 & \alpha_2 = .00385 \\ D[3] = 100.000 & \alpha_3 = .00385 \end{array}$$

other matrices are:

A[*]	Accumulates sums used to calculate aerosol spectrum polynomial
B[*]	Designates plotting symbols for various aerosol radii ranges
D	Data file number
C[*]	Data file bookkeeping as given below
E[*]	Aerosol radii bin centers
F[*]	Accumulates sums used to calculate aerosol spectrum polynomial
G[*]	Coefficients of polynomial fit
H[*]	Analog and digital signals from PMS housekeeping modules
M[*]	Aerosol curve fitting extrapolation sums
N[*]	PMS range counter
O[*]	Temporary dN/dr
R[*]	Aerosol radii bin edges
S[*]	Aerosol raw counts (dN)
T[*]	dN/dr
V[*]	Sums for calculating $\sigma(u)$ and $\sigma(\bar{v})$
W[*]	Sampling area versus bin for OAP
X[*]	Designates aerosol bins to be excluded from various considerations
Y[*]	Date and time
Z[*]	Mostly scaling parameters (see below)

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### File Bookkeeping

C[1] No. of files available on track 0 of cassette  
C[2] No. of files available on track 1 of cassette  
C[3] Data Tape No.

### The Components of Z[\*] are:

Z[1] Z; distance from waterline to sensors (28 meters for STREX)  
Z[2]  $Q_s$   
Z[3]  $Q$   
Z[4]  $U_*$   
Z[5]  $T_*$   
Z[6]  $q_*$   
Z[7]  $\epsilon$   
Z[8]  $U_*\epsilon$   
Z[9] True wind speed  
Z[10] Z/L  
Z[11] RH from dew pointer

### Strings output to files

T\$ dN/dr  
H\$ Analog and digital outputs from PMS housekeeping  
Y\$ Date and time  
M\$ P[I,J]  
U\$ U[I,J]

### Special function keys

Key	Action	How Program Responds
1	*sfg1	Reset. Starts program from beginning
2	*cmf2	Plot Log (dV/dr) versus Log(r)
3	*sfg3	Print sensor status
4	*sfg4	Activate or deactivate a sensor
5	*sfg5	Change order of polynomial
6	*sfg6	Change averaging time
7	*cmf7	Skip all printing
8	*sfg8	Use PMS clock instead of HP clock
9	*sfg9	Print radii matrix
10	*sfg10	Mark a tape
11	*sfg11	Get RH from Hygroductics instead of dew pointer

## I. THE BDM CORPORATION

### II. Computer Program

The following program, in HPL, was used with an HP9825S calculator during STREX.

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## STREX METUAS PROGRAM

```

0: "METUAS STREX":sfg 14
1: dim AS[15,4],HS[128],MS[60],TS[480],US[60],YS[24],TH,B,Z[11]
2: dim QS[1300],ZS[10],CS[3]
3: dim A[10],B[10],D[3],E[8,15],F[10,10],G[10],H[4,8],K[3,5]
4: dim L[3,5],M[8],N[8],O[8,15],P[3,5],R[8,16],S[8,15],T[8,15]
5: dim U[3,5],V[2,3],W[2,15],X[8],Y[6]
6: 35*B[1];111*B[2];43*B[3];0*B[4];64*B[5];42*B[6];37*B[7];38*B[8]
7: for J=4 to 5;40*K[3,J]+L[3,J];next J
8: for J=1 to 5;J-1*K[1,J]+L[1,J];next J;5*K[2,1]+L[2,1];6*K[2,2]+L[2,2]
9: 10*K[2,3]+L[2,3];11*K[2,4]+L[2,4];15*K[2,5]+L[2,5]
10: for J=1 to 3;6+J*K[3,J]+L[3,J];next J
11: 99.5989*D[1];99.4823*D[2];99.4433*D[3]
12: "Wsd"→AS[1];"Wdir"→AS[2];"Sdir"→AS[3];"Sspd"→AS[4];"<V>"→AS[5]
13: "Trn"→AS[6];"RH"→AS[7];"IR1"→AS[8];"IR2"→AS[9];"Vrms"→AS[10]
14: "Tdew"→AS[11];"Tair"→AS[12];"Tsea"→AS[13]
15: .028*W[1,1];.217*W[1,2];.632*W[1,3];1.177*W[1,4];1.734*W[1,5]
16: 2.346*W[1,6];3.05*W[1,7];3.737*W[1,8];4.6*W[1,9];5.393*W[1,10]
17: 6.133*W[1,11];6.903*W[1,12];7.652*W[1,13];8.36*W[1,14];9.012*W[1,15]
18: 9.15*W[2,1];6.54*W[2,2];7.93*W[2,3];7.32*W[2,4];6.71*W[2,5]
19: 6.1*W[2,6];5.49*W[2,7];4.83*W[2,8];4.27*W[2,9];3.66*W[2,10]
20: 3.05*W[2,11];2.44*W[2,12];1.83*W[2,13];1.22*W[2,14];.61*W[2,15];28*Z[1]
21: wtc 9,0;rem 709;rem 711;rem 704;110 7;715+1;dev "A",M;ldk 1;buf "Q",QS,3
22: rem 722;wrt 704,"A55";wrt 722,"FLR4F2B3A0"
23: "formats":fmt 0,10x,z
24: fmt 1,f3.0
25: fmt 2,cl,f3.0,z
26: fmt 3,"Date",f3.0,"/",f2.0,"/",f2.0," Time ",f4.0,":",f2.0," (PST)."
27: fmt 4,"Averaging time = ",f4.1," minutes"," Nb. Averages ",f4.0
28: fmt 5,"Probe voltage A = ",f6.3," volts"
29: fmt 6,e10.2,z
30: fmt 7,"Tape #",f3.0," File #",f3.0," STREX"
31: fmt 8,"Polynomial of order ",f2.0,z
32: fmt 9,e15.7,z
33: "RESET":dso "SET ANY FLAGS (CONT).";sto
34: if flq10;cfq 10;gsb "tapemrk"
35: if flq4;cfq 4;gsb "SENSORS"
36: 7+C;if flq5;cfq 5;ent "ORDER OF POLYNOMIAL?" ,C
37: C+1+I;rdm A[I],G[I],F[I,I]
38: 30+T;int(3T)+Z;if flq6;cfq 6;ent "AVERAGING TIME?",T;int(3T)+Z
39: dso "INSERT DATA TAPE (CONT).";sto
40: ldf 0,D,C[*]
41: dso "TURN ON PFDITER(CONT).";sto
42: wtb M,27,69,27,84,32,32,32,32,27,77,27,76,15,0,14
43: wtb M,27,79,4,43,6,26
44: 3*X[1]+X[2]+X[3];1+X[5]+X[6];15*X[4];0+X[7]+X[8]
45: .0845*R[1,1];.0875*R[1,2];.0905*R[1,3];.094*R[1,4];.098*R[1,5]
46: .102*R[1,6];.1065*R[1,7];.111*R[1,8];.1155*R[1,9];.12*R[1,10]
47: for J=11 to 16;R[1,J-1]+.005*R[1,J];next J
48: for J=1 to 16;(.23+.025(J-1))/2*R[2,J]

```

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```

49: .2+.02(J-1)*R[3,J];.3+.08(J-1)*R[4,J];.25+.25(J-1)*R[5,J]
50: if R[5,J]>1;.767*R[5,J]+.233*R[5,J]
51: 1+(J-1)*R[6,J];.767*R[6,J]+.233*R[6,J];next J
52: for J=1 to 16;3.55+4.93(J-1)*R[7,J];77.5+5(J-1)*R[8,J];next J
53: for I=1 to 8;for J=1 to 15;(R[I,J+1]+R[I,J])/2+E[I,J];next J;next I
54: "start":int(3T)+Z;0+K+I+N;fxd 0;ina H,S,N,V,P
55: "data":buf "Q";tfr 9,"Q",1284;K+1+K
56: dso "DATA XFER #",K,"OF",Z;imp rds("Q")=1284
57: dso "PROC #",K,"FILE #",D,"MAX",C[1]+C[2]
58: cll 'R1'(Y[5]);c11 'R1'(Y[6]);c11 'R1'(A);c11 'R1'(B);10shf(B,4)+3
59: band(A,3)+A;band(3,3)+3
60: "loop":for J=1 to 10;for L=1 to 4;c11 'R2'(Q);if J>2;imp 5
61: if J=2;imp 5
62: if L>2;imp 4
63: int(Q/100)+Y[2L-1];100frc(Q/100)+Y[2L];if Y[1]#80;wait 5000;goto "data"
64: imp 2
65: Q+H[L,J-2]+H[L,J-2]
66: if L=1;4-A+3;imp 4
67: if L=2;if B<2;6+3;imp 3
68: if L=2;5+3;imp 2
69: L+4+3
70: for I=1 to 15;c11 'R2'(Q);Q+S[S,I]+S[S,I];next I
71: 1+N[S]+N[S];next L;next J;1+H+H;imp 4
72: "R1":0+n2;imp 2
73: "R2":band(cmpbdb("Q"),255)+n3;band(p3,15)+10shf(p3,4)+n2
74: band(cmpbdb("Q"),255)+n4;band(p4,15)+10shf(p4,4)+100n2+n1;ret
75: wait 50;wrt 704,"A56";wait 50;wrt 722,"F1R4F2A3A0";for L=1 to 5
76: for I=1 to 2;for J=1 to 5;if L[I,J]>39;imp 5
77: fmt f3.0;wrt 709,"C",L[I,J];wait 5
78: trg 722;fmt f;red 722,F;F+P[I,J]+P[I,J]
79: if I=1;if J=1;F+V[1,1]+V[1,1];imp 2
80: if I=1;if J=5;F+V[2,1]+V[2,1]
81: next J;next I;1+N+N
82: c11 'AVEDEGS'(P[1,2],U[1,2],N);c11 'AVEDEGS'(P[1,3],U[1,3],N)
83: next L;c11 'SIGMA'
84: wrt 704,"B56"
85: wait 50;wrt 722,"F5R1T2M3A0";for J=1 to 3;if L[3,J]>39;imp 3
86: fmt 2f3.0;wrt 709,I[3,J]+5,L[3,J];wait 5;trg 722;fmt f;red 722,F
87: F+P[3,J]+P[3,J];wrt 709,"C";if F<100;if F>110;stp
88: next J;if K<Z;goto "data"
89: fmt 2x,c10;red 708,Z5
90: "****MET CALCULATIONS****":
91: for I=1 to 2;for J=1 to 5;if L[I,J]>39;imp 2
92: P[I,J]/N+P[I,J]
93: next J;next I;for J=1 to 3;if L[3,J]>39;imp 2
94: P[3,J]*5/N+P[3,J]
95: next J;P[1,5]+U[1,5];P[2,5]+U[2,5]
96: "FOUR WIRES":.003892+r1;(P[3,1]-D[1])/r1D[1]+U[3,1]
97: .00385+r1;for I=2 to 3;if L[3,I]>39;imp 2
98: (P[3,I]-D[I])/r1D[I]+U[3,I]
99: next I
*12117

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100: for I=3 to 4;10(P[2,I]-1)*U[2,I];next I
101: 8P[1,4]*U[1,4]
102: 10P[1,1]*U[1,1]
103: 100P[2,1]*U[2,1]
104: for I=1 to 2;((V[I,3]-V[I,2]^2/H)/(H-1))^*.5*V[I,1];next I
105: 5.14V[1,1]*V[1,1]
106: U[1,2]*R;U[1,1]*V;U[1,4]*S
107: deq;sqrt(V^2+S^2-2VScos(R))+r1;.514r1*U[3,4]+Z[9];vsin(R)/r1*r2
108: (-S+Wcos(R))/r1*r3;if r3>0;asn(r2)*U[3,5];jmp 3
109: if r2>0;acs(r3)*U[3,5];jmp 2
110: 180-asn(r2)*U[3,5]
111: (U[3,5]+U[1,3])mod360*U[3,5];cll 'SCALCALC'
112: for I=1 to 4;.26N[I]*N[I];next I;30.4N[5]*N[5];30.4N[6]*N[6]
113: for I=7 to 8;13.45*2N[I]*N[I];next I
114: for I=1 to 5;for J=1 to 15;if S[I,J]=0;1+S[I,J]
115: next J;next I
116: for I=1 to 6;for J=1 to 15;S[I,J]/N[I]*T[I,J];next J;next I
117: for I=7 to 8;for J=1 to 15;S[I,J]/(W[I-6,J]*H[I])*F[I,J];next J;next I
118: for I=1 to 4;for J=1 to 8;H[I,J]/1000/H+H[I,J];next J;next I
119: for I=1 to 8;for J=1 to 15;T[I,J]/(R[I,J+1]-R[I,J])*T[I,J]+O[I,J]
120: next J;next I
121: "nat":ina A,F;for I=1 to 8;if I=1 or I=6;0+r1+r2+r3+r4+r5+r6+r7+r8+r9
122: for J=X[I]+1 to 16;1+G;if J<16;jmp 5
123: if I>1 and I<6;gto "nExt"
124: if I=1;-1.5*X;gto "1"
125: if I=8 and r9#0 and r7#0;log(r8/r9)*X;log(r7/r9)*P;1+r5;gto "3"
126: 2.2*X;gto "1"
127: if O[I,J]=0 and I<6;gto "nExt"
128: 4*pi/3*E[I,J]^3*O[I,J]+O[I,J]
129: if r9#0;gto "extran"
130: if O[I,J]=0 and I>5;gto "extran"
131: log(O[I,J])*P;log(E[I,J])*X
132: if I=1 and J<9;gto "3"
133: if I<6;gto "2"
134: gto "3"
135: "extran":r9+1+r9;r7+O[I,J]+r7;r8+F[I,J]+r8;gto "nExt"
136: "3":r0+XX*r0;r1+X*r1;r2+1+r2;r3+PX*r3;r4+P*r4;if r5=0;gto "2"
137: X+2[9];P+2[10];1.5*X
138: "1":(r3r2-r4r1)/(r0r2-r1r1)*M[2]
139: (r0r4-r3r1)/(r0r2-r1r1)*M[1];M[1]+M[2]*X+P
140: "2":for K=0 to C;C+1-K*R;G+F[R,R]*F[R,R]
141: P+A[R]*A[R];P*X+P;GX+G
142: if K#C;G+F[R-1,R]*F[P-1,R]
143: G*X+3;next K
144: "nExt":next J;next I;if r5#0;sfg 12
145: for I=1 to C+1
146: for K=1 to int((C+1)/2)
147: if I#1 and I+K<C+2 and I-K>0;F[I,I]*F[I-K,I+K]+F[I+K,I-K]
148: if I+K<C+1 and I-K+1>0;F[I,I+1]*F[I+K,I-K+1]
149: if I+K<C and I-K>0;F[I,I+1]*F[I-K,I+K+1]
150: next K;next I;inv F=F;mat FA=G

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# THE BDM CORPORATION

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151: "olt":D+E;D+1+D;rcf 0,D,C[*];if D-1X[1];trk 1;D-C[1]-2+E
152: fdf E;if flg7;gto "SKIP PRINT"
153: "out":wrt "M.7",C[3],D-1;if flg8;jmp 3
154: 80+Y[1];val(ZS[1,2])→Y[2];val(ZS[3,4])→Y[3];val(ZS[5,6])→Y[4]
155: val(ZS[7,8])→Y[5];val(ZS[9,10])→Y[6]
156: wrt "M.3",Y[2],Y[3],Y[1],100Y[4]+Y[5],Y[6]
157: wrt "M.4",F;wrt "M.5",H[1,1];wtb M,10,13;if flg0;ret
158: fmt 11x,c5,15x,c9,11x,c14,z;wrt "1", "Ship", "true wind", "Relative wind"
159: wtb M,13;c11 'SPACE'(7)
160: for I=1 to 3;for J=1 to 13;wtb M,95;next J;c11 'SPACE'(10);next I
161: fmt /,4x,c11,f5.1,7x,c11,f5.1,7x,c11,f5.1,;U[3,4]/.514→r1
162: wrt "M", "Speed(kts):",U[1,4], "Speed(kts):",r1, "Speed(kts):",U[1,1]
163: fmt 7x,c8,f5.0,10x,c8,f5.0,10x,c8,f5.0,/
164: wrt "M", "Heading:",U[1,3], "Heading:",U[3,5], "Heading:",U[1,2]
165: fmt 3x,c2,6x,c2,6x,c2,5x,c4,4x,c4,7x,c3,7x,c2,7x,c,z
166: wrt "M", "Is", "Ta", "Td", "Tirl", "Tir2", "Z/L", "RH", "B"
167: fmt 6x,c,6x,c4,5x,c2,5x,c3,z;wrt "M", "V", "Vrms", "U*", "U*e"
168: wtb M,13;for I=1 to 100;wtb M,95;next I;wtb M,10,13
169: fmt x,f5.2,2x,f6.2,2x,f6.2,2x,f6.2,x,f10.2,2x,f6.2,4x,f5.1,z
170: Z[11]→r1;if flg11;U[2,2]→r1
171: wrt "M",U[3,3],U[3,2],U[3,1],U[2,3],U[2,4],Z[10],r1,B
172: fmt 2x,f5.1,3x,f5.1,2x,f6.3,2x,f6.3
173: wrt "M",U[1,5],U[2,5],Z[4],Z[8]
174: wtb M,10,"Raw Counts",10,13;for J=1 to 15;for I=1 to 8
175: wrt "M.6",S[I,J];next I;wtb M,10,13;next J;wtb M,10,13
176: wtb M,"dv/dr",10,13;for J=1 to 15;for I=1 to 3;wrt "M.6",F[I,J]
177: next I;wtb M,10,13;next J;wtb M,10,13
178: if not flg9;jmp 3
179: wto M,"Radii";wtb M,10,13;for J=1 to 15;for I=1 to 3;wrt "M.6",S[I,J]
180: next I;wtb M,10,13;next J;wtb M,10,13;cfg 9
181: if not flg2;wtb M,12;gto "SKIP PRINT"
182: sfq 0;wtb M,12,13;c11 'out';cfg 0;wtb M,27,65,-4,0,7,32,"log(dv/dr)"
183: wtb M,27,65,1,56,7,32;wrt "M.8",C;5.01-1/6→Y
184: for I=1 to C+1;wtb M,27,65,1,56,int(3Y/2),int(96Y)
185: wrt "M.9",S[I];Y-1/6→Y;next I
186: wtb M,27,65,-4,-210,-1,-16,"log(radius)"
187: -1→X;-4→Y
188: wtb M,27,65,int(15X/4),int(240X),0,0
189: if X#0 and Xmod1=0;wtb M,"|",10,8,8,8;wrt "M.1",X;gto +2
190: wtb M,"-"
191: if (X+.05→X)<2.3;gto -3
192: wtb M,27,65,0,0,int(1.5Y),int(96Y)
193: if Y#0 and Ymod1=0;wrt "M.2", "-",Y;gto +2
194: wtb M,"|"
195: if (Y+.1→Y)<5.1;gto -3
196: for I=1 to 8;for J=X[I]+1 to 15
197: if E[I,J]=0 or O[I,J]=0;gto "NEXT"
198: log(E[I,J])→X;log(O[I,J])→Y
199: wtb M,27,65,int(15X/4),int(240X),int(3Y/2),int(96Y)
200: wtb M,S[I]
201: "NEXT":next J;next I;if not flg12;jmp 2

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# THE BDM CORPORATION

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202: wtb M,27,65,int(15B[9]/4),int(240B[9]),int(3B[10]/2),int(96B[10]),"e"
203: -1→X;0→Y;cfq 12
204: "crv":0→Y;if X>2;gto "belch"
205: for I=1 to C+1;YX+G[I]→Y;next I
206: Y→M[4];jmp 3
207: "belch":if X>2.1;if M[2]>0;M[6]→Y;jmp 2
208: M[4]+M[2]*(X-2)→Y→M[6]
209: if Y<-4 or Y>5;jmp 4
210: Y+6/96→Y
211: wtb M,27,65,int(15X/4),int(240X),int(3Y/2),int(96Y)
212: wtb M,"."
213: if (X+1/120→X)<2.2;gto "crv"
214: wtb M,10,12,13
215: "SKIP PRINT":for I=1 to 4;for J=1 to 8
216: 32(I-1)→K;fts (H[I,J])→HS[K+4J-3,K+4J];next J;next I;for I=1 to 8
217: for J=1 to 15;60(I-1)→K;fts (T[I,J])→TS[K+4J-3,K+4J];next J;next I
218: for I=1 to 6;fts (Y[I])→YS[4I-3,4I];next I
219: for I=1 to 3;for J=1 to 5;20(I-1)→K;fts (P[I,J])→PS[4J-3+K,4J+K]
220: fts (U[I,J])→US[4J-3+K,4J+K];next J;next I
221: if flg7;dso "FILE",L,"PRINT SUPPRESSED";jmp 2
222: dso "RECORDING FILE",D-1,"MAX. NO.",C[1]+C[2]
223: if DX[C[1]+C[2]];c11 'tapemrk'
224: rcf E,HS,NS,TS,US,YS,T,H,E,Z[*];trk 0;fdf 0
225: "FLACS":if flg1;cfq 1;gto "FSET"
226: if flg5;cfq 5;dso "Poly=",C,"New=";ent "",C;C+1→R;rdm A[R],G[R],F[R,S]
227: if flg6;cfq 6;dso "Averaging time=",T,"New=";ent "",T;int(3T)→Z
228: if flg3;cfq 3;c11 'SENSOR STATUS'
229: gto "start"
230: "tapemrk":for I=1 to 5;beep;wait 500;next I
231: dso "Insert new cassette,continue.";sto
232: dso "Are you sure?Continue.";sto
233: ent "Tape number?",C[3]
234: trk 0;rew;mrk 129,950;rew;128→C[1]+C[2];1→D
235: rcf 0,0,C[*];rew;trk 1;mrk 129,950;rew;trk 0;ret
236: "AVEDEGS":72p1→p1;p1-p2→p4;abs(p4)→p5
237: if p5>=180;(p4/p5)(p5-360)→p6;(p6/p3+p2)mod360→p2;jmp 2
238: p2→p4/p3→p2
239: 0→p1;ret
240: "SENSOR STATUS":prt "SENSOR STATUS";prt "DEACTIVATED"
241: prt Z$[1,2]&"/"&Z$[3,4]&" at "&Z$[5,8]
242: for I=1 to 3;for J=1 to 5;if L[I,J]>40;prt AS[5(I-1)+J]
243: next J;next I;ret
244: "SENSORS":ent "ACTIVATE(a),DEACTIVATE(d) OR (f)",CS;if CS="f";ret
245: if CS#"a" and CS#"d";beep;jmp -1
246: ent "SENSOR NAME",US;if US="f";jmp -2
247: for I=1 to 3;for J=1 to 5;if US=AS[5(I-1)+J];jmp 2
248: next J;next I;beep;jmp -2
249: if CS="d";41→L[I,J];jmp -3
250: K[I,J]→L[I,J];jmp -4
251: "SIGMA":for I=1 to 2;V[I,1]/(L-1)→C;C+V[I,2]→V[I,2]
252: 0→Q+V[I,3]→V[I,3];0→V[I,1];next I;ret

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# THE BDM CORPORATION

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253: "SCALCALC":Z[9]→r1;U[3,3]→r2;U[3,2]→r3;U[3,1]→r4;rad
254: if r1<.01;ina Z;28→Z[1];ret
255: if r1<2.2;.001*1.08*r1^(-.15)→r5;jmp 4
256: if r1<5;.001*(.77+.086*r1)→r5;jmp 3
257: if r1<8;.001*(.87+.067*r1)→r5;jmp 2
258: .001*(1.2+.025*r1)→r5
259: 10*exp(-.35/r5^5)→r6;ln(Z[1]/r6)→r7;ln(Z[1]/.00002)→r8
260: cll 'Q'(r2,Z[2]);c11 'Q'(r3,r20);if flg11;.01*U[2,2]*r20+Z[3];jmp 2
261: cll 'Q'(r4,Z[3]);Z[3]/r20*100→Z[11]
262: 9.8*.35*Z[1]/(r3+273.15)*(.35*1.35/r8)/(.35/r7)^2→r9
263: r9*(r3-r2+.01*Z[1]+.00061*(r3+273.15)*(Z[3]-Z[2]))/r1^2→r9+r10
264: if r9>2.2;50→r13;c11 'PSI1'(r13,r11);c11 'PSI2'(r13,r12);gto 267
265: c11 'PSI1'(r10,r11);c11 'PSI2'(r10,r12);r9*(1-r11/r7)^2/(1-r12/r3)→r13
266: fxd 3;dsp r10,r13;if abs(r10-r13)>.001*abs(r9);r13→r10;jmp -1
267: r13→Z[10];.35/r7*r1/(1-r11/r7)→Z[4]
268: .35*1.35/r8*(r3-r2+.01*Z[1])/(1-r12/r3)→Z[5]
269: .35*1.35/r8*(Z[3]-Z[2])/(1-r12/r8)→Z[6]
270: 4U[1,5]√(.514U[1,1])V[2,1]/V[1,1]→Z
271: 4.463e-3*(.514U[1,1])^5(U[1,5]U[2,5]/3)^3→Z[7]
272: c11 'PHIEPS'(r13,r14);(Z[7]*.35*Z[1]/r14)^.333→Z[8]
273: ret
274: "PSI1":if p1>0;-4.7*p1→p2;ret
275: (1-15*p1)^.25→p2;2*ln((1+p2)/2)+ln((1+p2^2)/2)-2*atn(p2)+1.64→p2;ret
276: "PSI2":if p1>0;-6.5*p1→p2;ret
277: (1-9*p1)^.5→p2;2*ln((1+p2)/2)→p2;ret
278: "PHIEPS":if p1>0;(1+2.5*p1^67)^1.5→p2;ret
279: (1+.5*abs(p1)^67)^1.5→p2;ret
280: "Q":.625*10^(23.84-2948/(r1+273.15)-5.03*log(p1+273.15))→p2;ret
281: "SPACE":wth "M",32;jmp (p1-1→r1)=0
282: ret
*16632

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THE BDM CORPORATION

APPENDIX B  
SUMMARY OF METEOROLOGICAL DATA FOR STREX

In the summary of met data for STREX, the headings have the following meaning:

HEADING	QUANTITY	UNITS
TIME		PST
U	True Wind Speed	m/sec
RDir	Relative Wind Direction	deg
T <sub>s</sub>	Sea Surface Temperature	°C
T <sub>a</sub>	Air Temperature	°C
T <sub>d</sub>	Dew Point	°C
T <sub>ir</sub>	Infrared Sea Surface Temperature	°C
Z/L	Similarity Height Parameter	-
RH	Relative Humidity	-
B	Hot Film Sensitivity	Volts <sup>2</sup> /(m/sec) <sup>1/2</sup>
V	Mean Hot Film Voltage	Volts
V <sub>rms</sub>	Root Mean Square Hot Film Voltage	Volts
U <sub>*</sub>	Friction Velocity	m/sec
U <sub>*ε</sub>	Friction Velocity Based on Dissipation Rate	m/sec

# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 1

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	U*	Ute	
1	11/ 5	1543:16	4.5	344	11.92	10.23	7.57		-0.96	83.56	17.3	8.0	0.5	0.153	0.100	
2	11/ 5	1703:36	7.6	19	11.69	10.80	9.03		-0.14	88.85	14.7	7.8	0.6	0.266	0.158	R30
3	11/ 5	1735:56	13.8	38	11.59	11.21	9.98		-0.01	92.15	16.2	8.6	1.4	0.490	0.399	R 5
4	11/ 5	1808:16	16.5	35	11.41	11.16	10.03		-0.00	92.79	14.5	8.9	1.3	0.598	0.464	
5	11/ 5	1840:36	16.8	30	11.38	11.12	9.82		-0.00	91.70	14.3	9.0	1.3	0.610	0.453	
6	11/ 5	1912:56	16.4	28	11.26	10.87	9.65		-0.01	92.20	15.7	9.1	1.5	0.596	0.470	
7	11/ 5	1941:56	15.8	27	11.10	10.20	8.33		-0.03	88.20	15.1	9.1	2.3	0.575	0.762	R16
8	11/ 5	2012:36	14.5	24	10.72	10.00	7.68		-0.03	85.53	17.2	8.9	2.4	0.521	0.673	R30
9	11/ 5	2044:36	15.5	19	10.73	10.21	8.38		-0.02	88.41	16.5	9.1	1.5	0.560	0.450	R 3
10	11/ 5	2116:56	15.5	25	10.78	9.73	8.70		-0.03	93.32	15.9	9.1	1.3	0.565	0.396	
11	11/ 5	2149:17	14.2	28	10.74	10.18	7.83		-0.02	85.35	14.6	8.9	1.0	0.508	0.337	
12	11/ 5	2221:37	12.4	26	11.24	10.18	7.48		-0.06	83.33	15.4	8.7	1.3	0.443	0.388	R 9
13	11/ 5	2253:57	10.4	18	10.68	10.13	7.67		-0.05	84.67	16.0	8.6	0.7	0.365	0.188	
14	11/ 5	2326:17	9.3	11	10.70	9.79	7.46		-0.10	85.41	15.8	8.5	0.7	0.329	0.187	
15	11/ 5	2358:37	9.2	14	10.57	9.81	7.74		-0.08	86.95	15.8	8.5	0.6	0.322	0.171	
16	11/ 6	30:57	8.4	18	10.42	9.78	7.52		-0.08	85.79	17.3	8.2	0.6	0.293	0.136	
17	11/ 6	103:17	8.6	25	10.42	9.64	7.29		-0.10	85.28	17.5	8.2	0.6	0.302	0.140	
18	11/ 6	135:37	7.8	27	11.01	9.54	7.04		-0.23	84.41	16.4	7.9	1.1	0.278	0.234	R15
19	11/ 6	207:57	6.5	27	10.38	9.47	6.55		-0.23	81.99	17.3	7.5	0.7	0.222	0.139	R 1
20	11/ 6	240:17	7.1	41	10.27	9.42	6.49		-0.17	81.93	19.3	7.3	0.8	0.245	0.129	
21	11/ 6	312:37	6.3	39	10.19	9.39	6.09		-0.22	79.86	20.3	7.0	1.0	0.214	0.135	
22	11/ 6	344:57	6.7	59	10.18	9.34	5.81		-0.20	78.58	20.7	6.7	1.1	0.229	0.136	
23	11/ 6	417:17	6.9	85	10.10	9.30	5.39		-0.19	76.56	18.1	6.7	1.3	0.237	0.172	*
24	11/ 6	449:37	7.6	101	10.05	9.26	5.32		-0.14	76.35	12.2	7.0	1.5	0.267	0.322	*
25	11/ 6	521:57	8.8	108	10.05	8.84	5.50		-0.16	79.61	12.3	7.3	2.3	0.310	0.556	R14 *
26	11/ 6	554:17	8.8	103	10.11	9.18	5.78		-0.12	79.33	8.1	7.5	1.7	0.311	0.651	*
27	11/ 6	626:37	10.8	9	10.11	9.18	5.67		-0.08	78.73	19.7	9.0	1.3	0.383	0.289	
28	11/ 6	658:57	11.7	350	10.13	9.21	6.02		-0.06	80.49	17.2	9.1	1.3	0.418	0.341	
29	11/ 6	731:17	11.3	3	10.13	9.17	6.72		-0.07	84.66	13.1	8.8	1.3	0.403	0.448	
30	11/ 6	803:37	11.5	59	10.93	9.10	6.83		-0.13	85.72	10.9	8.5	2.6	0.414	0.970	R18
31	11/ 6	913:37	13.8	53	11.20	7.29	4.32		-0.19	81.44	13.1	8.2	4.8	0.512	1.483	R30
32	11/ 6	945:57	13.4	53	11.05	8.71	6.80		-0.12	87.76	8.3	8.3	2.1	0.490	1.069	R 2
33	11/ 6	1021:17	13.6	49	9.96	8.84	6.05		-0.06	82.64	11.3	8.2	1.3	0.490	0.496	
34	11/ 6	1053:37	14.6	44	9.90	8.75	6.19		-0.05	83.98	15.8	8.4	1.3	0.529	0.351	
35	11/ 6	1125:57	14.4	43	9.87	8.69	6.04		-0.05	83.43	22.4	8.3	1.2	0.520	0.240	
37	11/ 6	1308:17	9.7	337	9.86	9.36	5.76		-0.05	78.22	15.7	7.4	1.5	0.338	0.349	V 3
38	11/ 6	1340:38	7.8	203	9.87	9.38	6.02		-0.08	79.52	32.7	6.1	9.0	0.272	0.734	*
39	11/ 6	1412:58	7.5	209	9.87	9.23	6.14		-0.11	80.99	29.8	5.8	9.6	0.260	0.786	*
40	11/ 6	1445:18	6.9	204	9.88	8.98	6.49		-0.19	84.38	20.3	6.0	8.4	0.238	0.966	*
41	11/ 6	1920:38	7.7	316	9.91	9.65	7.14		-0.04	84.38	16.5	8.0	7.5	0.264	1.933	V30
42	11/ 6	1952:58	8.1	318	9.97	9.45	7.40		-0.07	87.01	23.7	8.1	6.9	0.280	1.237	V30
43	11/ 6	2025:18	8.0	314	10.03	9.65	7.15		-0.05	84.46	14.7	7.9	8.0	0.276	2.259	V30
44	11/ 6	2057:38	9.9	318	10.80	9.59	7.06		-0.12	84.20	34.8	7.8	4.8	0.352	0.554	V23
45	11/ 6	2129:58	10.9	219	9.94	9.34	7.40		-0.04	87.67	8.4	7.4	4.5	0.383	1.988	*
46	11/ 6	2202:18	10.8	160	9.84	9.32	7.44		-0.03	88.00	5.6	7.4	3.9	0.377	2.402	*
47	11/ 6	2234:38	13.0	22	9.90	9.30	7.44		-0.03	88.18	14.8	7.9	3.0	0.464	0.853	V30

# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 1

FILE	DATE	TIME	U	RDir	Ts	Tq	Td	Tir	Z/L	RH	B	V	Vrms	U*	U**	
48	11/ 6	2306:58	11.3	317	9.87	9.22	7.08		-0.04	86.48	14.7	8.1	7.1	0.480	2.146	V30
49	11/ 6	2339:38	10.6	313	9.79	9.19	6.84		-0.05	85.25	15.8	8.1	8.1	0.372	2.253	V30
50	11/ 7	11:58	8.2	331	9.80	9.39	6.54		-0.06	82.37	9.5	7.7	6.4	0.284	2.671	V30
51	11/ 7	44:18	12.0	243	9.78	9.11	6.69		-0.04	84.85	12.7	7.8	5.5	0.426	1.751	*
52	11/ 7	116:38	13.1	53	9.77	8.96	6.60		-0.04	85.19	10.9	7.8	4.6	0.470	1.717	V30
53	11/ 7	148:58	16.7	32	9.79	9.20	6.36		-0.02	82.36	16.8	8.1	1.8	0.610	0.496	V 2
54	11/ 7	221:38	16.0	359	9.78	8.97	6.76		-0.03	86.83	13.2	8.5	1.6	0.582	0.595	
55	11/ 7	253:58	12.0	331	9.78	9.11	8.02		-0.03	92.87	15.1	8.3	4.1	0.424	1.225	V16
56	11/ 7	326:18	6.7	332	9.83	9.19	7.56		-0.12	89.53	15.9	7.4	5.1	0.229	1.162	V18
57	11/ 7	559:38	14.9	81	9.76	9.44	6.47		-0.01	81.70	7.9	8.1	2.8	0.536	1.521	R 3 *
58	11/ 7	1014:35	17.4	355	10.11	8.66	3.79		-0.05	71.48	13.0	8.0	2.0	0.644	0.678	R 4 V 1
59	11/ 7	1846:55	16.6	350	10.12	8.70	4.81		-0.05	72.38	18.3	7.6	1.6	0.612	0.371	
60	11/ 7	1119:15	16.6	338	10.12	8.40	4.10		-0.06	74.33	12.7	7.6	1.6	0.611	0.512	
61	11/ 7	1151:35	16.4	355	10.12	8.07	4.00		-0.07	75.52	12.5	7.6	2.0	0.604	0.677	V 5
62	11/ 7	1223:55	15.3	6	11.11	7.46	3.88		-0.14	78.88	13.4	7.6	2.3	0.570	0.666	R 3
63	11/ 7	1256:15	14.9	3	10.13	7.81	3.19		-0.10	72.62	12.3	7.4	1.6	0.548	0.520	
64	11/ 7	1328:35	14.3	354	10.12	7.63	2.56		-0.12	70.29	16.0	7.4	2.0	0.526	0.475	V 5
65	11/ 7	1400:55	15.4	3	10.12	7.84	1.55		-0.09	64.47	13.4	7.4	1.4	0.568	0.406	
66	11/ 7	1435: 1	14.8	356	11.63	7.68	0.36		-0.18	59.81	60.7	7.4	2.8	0.551	0.179	R13
67	11/ 7	1612: 1	12.9	12	10.14	7.47	1.97		-0.16	68.12	13.5	7.1	1.0	0.473	0.271	
68	11/ 7	1644:21	12.8	21	10.12	7.35	1.79		-0.17	67.80	16.6	7.2	1.2	0.478	0.254	
69	11/ 7	1716:41	11.5	48	10.12	7.24	2.04		-0.21	69.51	12.8	7.4	1.2	0.422	0.333	
70	11/ 7	1749: 1	11.9	19	10.13	6.63	1.92		-0.24	71.86	15.7	7.3	1.4	0.437	0.318	
71	11/ 7	1821:21	12.0	14	10.12	7.01	2.03		-0.21	70.62	10.9	7.2	1.8	0.439	0.578	R 3
72	11/ 7	1853:41	10.3	9	10.11	6.91	1.42		-0.30	68.85	11.5	7.0	1.1	0.378	0.316	
73	11/ 7	1926: 1	10.8	6	10.11	7.27	1.08		-0.25	64.82	19.5	7.2	1.1	0.394	0.205	R 2
74	11/ 7	1958:20	11.0	13	10.11	7.11	1.13		-0.25	65.75	14.4	7.9	1.2	0.402	0.325	
75	11/ 7	2054: 0	11.4	14	10.14	7.21	0.83		-0.23	63.91	14.3	8.0	1.2	0.418	0.321	
76	11/ 7	2126:21	10.5	3	10.14	7.00	0.87		-0.28	65.01	15.8	7.9	1.2	0.385	0.280	
77	11/ 7	2158:41	9.9	4	10.18	7.01	0.79		-0.33	64.58	14.4	7.8	1.1	0.361	0.281	
78	11/ 7	2231: 1	10.4	4	10.18	6.99	0.89		-0.30	65.10	17.8	7.8	1.8	0.381	0.369	R 7
79	11/ 7	2303:21	9.9	357	10.19	6.94	1.83		-0.33	69.93	14.2	7.7	1.2	0.364	0.302	
80	11/ 7	2335:41	9.0	245	10.14	7.22	0.52		-0.37	62.41	18.4	6.7	7.2	0.330	1.108	*
81	11/ 8	8: 1	9.1	226	10.13	7.22	0.53		-0.36	62.50	32.7	6.7	6.4	0.331	0.537	*
82	11/ 8	40:21	9.2	355	10.09	7.24	1.21		-0.35	65.54	28.9	7.6	3.3	0.334	0.405	V 8
83	11/ 8	112:41	10.1	26	10.12	6.79	1.76		-0.32	70.29	15.8	7.7	1.3	0.370	0.295	
84	11/ 8	145: 1	9.4	17	11.29	6.72	1.68		-0.51	70.23	18.1	7.5	2.1	0.349	0.383	R 9
85	11/ 8	217:21	9.4	6	10.15	7.02	1.78		-0.35	69.30	18.1	7.5	1.2	0.345	0.222	
86	11/ 8	249:41	10.2	5	10.14	7.15	0.89		-0.29	64.41	15.2	7.6	1.8	0.372	0.422	R 6
87	11/ 8	322: 1	10.6	13	10.14	7.10	1.05		-0.27	65.40	15.1	7.8	1.2	0.389	0.301	
88	11/ 8	354:21	10.5	9	10.13	7.02	1.21		-0.28	66.50	17.2	7.8	1.2	0.385	0.259	
89	11/ 8	426:41	9.6	194	10.10	7.18	1.70		-0.32	68.14	18.5	7.0	2.4	0.349	0.384	*
90	11/ 8	459: 1	11.1	12	10.08	7.22	0.95		-0.23	64.38	15.1	8.0	1.2	0.405	0.388	
91	11/ 8	531:21	10.6	11	10.12	6.83	0.96		-0.29	66.21	16.1	8.0	1.2	0.390	0.283	V 1
92	11/ 8	603:41	11.9	195	10.07	7.36	1.23		-0.19	65.10	13.2	7.1	4.2	0.435	1.000	*
93	11/ 8	636: 1	11.8	191	10.12	7.02	1.50		-0.22	67.89	15.4	7.7	2.2	0.433	0.518	*

# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 1

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	U#	Ute	
94	11/ 8	708:21	9.8	217	10.16	7.15	0.98		-0.32	64.83	15.1	6.6	2.3	0.359	0.418	*
95	11/ 8	740:41	11.6	298	10.76	7.11	0.95		-0.27	64.89	16.3	7.9	5.0	0.428	1.197	R20 *
96	11/ 8	959: 1	10.1	12	11.08	6.89	1.80		-0.40	70.02	14.6	7.7	1.4	0.374	0.342	R 6
97	11/ 8	1031:21	9.9	14	10.14	6.69	1.06		-0.35	67.30	15.2	7.7	1.4	0.363	0.328	R 1
98	11/ 8	1103:41	10.5	11	10.17	6.80	1.52		-0.30	69.05	13.5	7.8	1.1	0.384	0.299	
99	11/ 8	1517: 2	10.4	1	10.17	5.82	1.69		-0.38	74.79	10.3	8.0	1.5	0.387	0.303	
100	11/ 8	1549:22	10.3	344	10.17	6.90	-0.25		-0.31	60.33	17.8	7.9	1.3	0.379	0.270	
101	11/ 8	1621:42	12.1	344	10.18	6.89	0.94		-0.22	65.84	15.4	8.2	1.3	0.447	0.352	
102	11/ 8	1654: 2	12.0	4	10.18	6.37	0.97		-0.26	68.39	16.4	8.1	1.4	0.442	0.346	
103	11/ 8	1726:22	10.9	16	10.15	6.13	1.46		-0.33	72.00	14.2	7.9	1.4	0.403	0.360	
104	11/ 8	1758:42	10.6	272	10.15	5.77	1.14		-0.37	72.12	16.6	7.8	3.3	0.394	0.726	R27 *
105	11/ 8	2248:42	9.3	121	10.07	6.00	-3.76		-0.40	46.88	7.4	7.6	1.8	0.342	0.790	*
106	11/ 8	2321: 2	7.5	98	10.16	6.92	-2.89		-0.62	49.64	9.8	7.3	1.3	0.275	0.384	*
107	11/ 8	2353:22	8.1	77	10.20	6.07	-0.00		-0.52	61.57	9.5	8.0	1.5	0.299	0.537	*
108	11/ 9	25:42	8.7	13	10.13	6.43	0.49		-0.49	65.78	16.5	8.4	0.9	0.321	0.226	
109	11/ 9	58: 2	9.3	15	10.03	6.66	0.86		-0.39	66.46	14.8	8.6	1.0	0.342	0.292	
110	11/ 9	130:22	10.7	13	10.12	6.68	0.95		-0.30	66.86	12.7	8.5	1.1	0.394	0.382	
111	11/ 9	202:42	9.9	5	10.08	6.71	0.74		-0.35	65.69	14.6	8.4	1.0	0.362	0.292	
112	11/ 9	235: 2	10.2	14	10.10	6.65	0.39		-0.33	64.28	14.5	8.2	1.2	0.375	0.330	
113	11/ 9	307:22	10.8	22	10.03	6.88	1.87		-0.27	70.41	13.2	8.5	1.2	0.395	0.384	
114	11/ 9	339:42	10.7	13	10.07	7.06	1.35		-0.26	67.02	15.1	8.4	1.1	0.392	0.297	
115	11/ 9	412: 2	12.1	20	10.20	6.74	1.11		-0.23	67.31	13.7	8.3	1.2	0.445	0.352	
116	11/ 9	444:23	10.9	258	10.15	7.06	0.66		-0.26	63.77	29.7	6.4	11.4	0.400	1.128	*
117	11/ 9	516:43	9.7	276	10.14	7.04	1.12		-0.33	65.99	29.5	7.0	9.9	0.355	1.071	*
118	11/ 9	549: 3	9.3	265	10.15	6.90	1.78		-0.38	69.85	22.4	6.8	8.0	0.340	1.067	*
119	11/ 9	621:23	11.9	197	10.20	6.57	1.56		-0.25	70.36	19.4	7.0	4.7	0.438	0.731	*
120	11/ 9	653:43	11.1	173	10.22	7.81	0.78		-0.20	61.08	16.0	6.8	2.5	0.405	0.460	*
121	11/ 9	726: 3	8.1	77	10.35	7.25	1.35		-0.48	66.15	16.0	7.5	1.8	0.298	0.364	*
122	11/ 9	1002: 3	10.1	358	10.33	7.59	1.69		-0.27	66.25	16.1	8.0	1.2	0.369	0.278	V 1
123	11/ 9	1034:23	11.2	356	10.24	7.24	2.07		-0.24	69.70	14.9	8.1	1.3	0.409	0.356	
124	11/ 9	1135:18	12.5	360	10.07	6.59	2.78		-0.21	76.63	15.5	8.3	1.4	0.460	0.383	
125	11/ 9	1207:38	9.8	101	10.10	6.46	2.70		-0.37	76.90	16.1	7.6	1.5	0.359	0.314	*
126	11/ 9	1349:57	9.7	3	12.05	7.51	3.07		-0.48	73.46	18.1	7.8	1.8	0.358	0.352	R16
127	11/ 9	1422:17	9.1	0	10.07	7.18	3.53		-0.34	77.60	22.1	7.9	1.4	0.332	0.224	
128	11/ 9	1454:37	9.0	8	10.04	7.30	3.64		-0.33	77.57	17.3	7.8	1.2	0.326	0.256	
129	11/ 9	1526:57	9.9	25	10.00	6.78	3.61		-0.32	80.21	17.1	7.9	1.3	0.362	0.285	
130	11/ 9	1559:17	8.5	29	9.98	6.50	3.33		-0.47	80.22	17.6	7.7	1.3	0.311	0.254	V 7
131	11/ 9	1631:37	6.7	325	9.99	6.83	3.07		-0.73	76.98	13.5	7.5	2.3	0.241	0.534	V15
132	11/ 9	1708:37	8.5	62	9.99	6.80	2.15		-0.44	72.20	14.5	7.6	1.4	0.311	0.317	*
133	11/ 9	1740:57	9.8	6	11.81	7.01	0.87		-0.49	64.95	12.4	8.0	3.6	0.366	1.064	V14
134	11/ 9	1813:17	11.3	31	9.94	6.79	0.20		-0.24	62.83	16.4	8.3	1.2	0.416	0.298	
135	11/ 9	1845:37	11.6	33	9.85	7.00	-1.58		-0.22	54.38	14.9	8.3	1.2	0.423	0.326	
136	11/ 9	1917:57	11.1	32	9.86	6.91	-3.87		-0.25	46.19	16.6	8.4	1.3	0.407	0.340	R 4
137	11/ 9	1950:17	9.2	30	9.89	6.77	-3.21		-0.39	48.98	13.8	8.1	1.0	0.339	0.277	
138	11/ 9	2022:37	10.2	29	9.95	6.68	-0.68		-0.32	59.38	17.2	8.3	1.0	0.375	0.239	
139	11/ 9	2054:58	12.1	41	9.88	6.04	0.93		-0.25	69.74	15.4	8.4	1.3	0.449	0.368	

# THE BDM CORPORATION

SUMMARY OF MET DATA FOR STREX  
DATA TAPE NO. 1

FILE	DATE	TIME	U	RDir	Ts	Tq	Td	Tir	Z/L	RH	B	V	Vrns	Ut	Ute
140	11/ 9	2127:18	9.8	31	9.99	6.46	0.73		-0.36	66.77	15.0	8.1	1.1	0.361	0.282
141	11/ 9	2159:38	12.6	29	10.00	6.52	0.41		-0.21	64.98	21.4	8.4	1.3	0.466	0.261
142	11/ 9	2231:58	6.5	213	10.05	5.96	1.57		-1.01	73.42	19.4	6.3	4.7	0.237	0.524 *
143	11/ 9	2304:18	10.4	243	9.98	6.58	1.38		-0.31	69.40	20.7	7.4	3.7	0.383	0.572 *
144	11/ 9	2336:38	10.6	172	9.90	6.16	1.59		-0.32	72.53	10.0	7.5	3.6	0.391	1.162 *
145	11/10	8:58	6.2	109	9.96	6.46	0.32		-0.99	64.80	12.4	7.7	1.9	0.223	0.424 *
146	11/10	41:17	8.1	100	9.98	7.05	0.42		-0.46	62.68	10.6	7.9	1.7	0.296	0.542 *
147	11/10	113:37	12.0	324	9.95	7.04	0.04		-0.20	61.03	16.7	8.7	8.1	0.441	2.178 V29
148	11/10	145:57	11.5	334	9.90	6.74	-0.14		-0.24	61.53	16.4	8.9	5.2	0.424	1.429 V30
149	11/10	218:17	12.0	334	9.86	7.09	-1.21		-0.20	55.54	15.2	8.7	5.4	0.439	1.620 V30
150	11/10	250:37	11.3	326	9.90	7.00	-2.01		-0.24	52.69	17.2	8.4	6.9	0.414	1.701 V30
151	11/10	322:57	11.6	323	9.97	6.91	-1.09		-0.23	56.69	78.3	7.8	7.1	0.425	0.353 V30
152	11/10	355:17	11.2	337	9.90	6.93	-1.46		-0.24	55.14	12.7	7.1	5.2	0.410	1.487 V26
153	11/10	427:37	12.0	3	9.92	6.85	-1.79		-0.22	54.13	10.1	7.0	1.0	0.441	0.352
154	11/10	459:57	13.2	14	9.85	6.73	-0.90		-0.18	58.23	9.8	7.1	1.0	0.487	0.370
155	11/10	532:17	11.7	14	9.92	6.58	-0.15		-0.24	62.15	9.7	7.0	1.1	0.431	0.408
156	11/10	604:37	11.5	5	9.88	6.72	0.12		-0.24	62.77	11.8	7.0	1.2	0.422	0.349 V 2
157	11/10	636:57	10.1	177	9.89	6.69	0.12		-0.31	62.92	11.4	5.8	2.2	0.371	0.469 *
158	11/10	709:17	9.6	172	9.92	7.62	-0.25		-0.27	57.48	10.7	5.5	2.6	0.349	0.548 *
159	11/10	741:37	10.1	149	11.49	6.80	-0.57		-0.45	59.38	9.7	5.8	2.0	0.377	0.492 R18 *
160	11/10	813:57	7.5	320	10.60	6.74	-0.23		-0.71	61.11	12.6	6.3	3.8	0.276	0.823 R30 V30
161	11/10	846:17	7.6	34	10.15	7.00	-1.76		-0.57	53.69	5.8	6.5	1.2	0.280	0.561 R 4 V 7
162	11/10	1012:17	6.8	10	9.83	6.96	-1.71		-0.69	53.99	15.1	7.6	0.9	0.245	0.193
163	11/10	1044:37	7.0	0	9.83	6.94	-0.45		-0.64	59.32	19.2	7.7	0.9	0.253	0.146
164	11/10	1116:57	6.2	1	9.81	6.99	-0.75		-0.81	57.83	14.9	7.5	1.0	0.225	0.202
165	11/10	1403:18	2.9	341	9.78	6.99	0.65		-4.21	64.03	16.7	6.8	3.4	0.102	0.398 V30
166	11/10	1435:38	2.5	313	9.76	6.99	0.70		-5.75	64.23	19.0	6.6	6.0	0.088	0.551 V30
167	11/10	1507:58	5.7	231	9.77	7.57	0.23		-0.78	59.70	37.7	5.7	7.8	0.204	0.401 *
168	11/10	1651:58	6.7	359	9.68	7.14	0.80		-0.62	64.06	16.9	7.5	1.1	0.240	0.201
169	11/10	1724:18	6.3	10	9.70	7.10	1.20		-0.73	66.11	16.0	7.4	0.9	0.224	0.166
170	11/10	1756:38	6.3	22	9.72	7.31	1.40		-0.66	66.12	14.0	7.5	0.9	0.225	0.204
171	11/10	1828:58	8.9	27	9.69	7.68	1.42		-0.27	64.55	13.7	8.4	0.8	0.322	0.234
172	11/10	2126:18	11.1	2	9.78	7.94	6.52		-0.13	90.73	14.9	7.8	1.4	0.400	0.353
173	11/10	2158:38	9.9	290	9.79	7.99	6.66		-0.17	91.27	35.6	7.3	10.0	0.355	0.997 *
174	11/10	2230:58	11.3	291	9.79	8.28	6.92		-0.10	91.15	18.6	7.7	10.5	0.405	2.195 *
175	11/10	2303:18	12.3	287	9.79	8.34	6.69		-0.09	89.32	30.9	7.7	11.0	0.440	1.394 *
176	11/10	2335:38	12.3	9	9.81	8.36	6.22		-0.09	86.40	13.4	8.0	2.4	0.443	0.734 V30
177	11/11	7:58	14.6	13	9.82	8.41	6.14		-0.06	85.63	13.1	8.1	2.0	0.531	0.645 V 4
178	11/11	40:18	14.3	211	9.79	8.53	6.87		-0.05	89.29	22.2	7.7	3.0	0.519	0.533 *
179	11/11	112:38	12.2	266	9.83	8.70	7.35		-0.06	91.21	12.4	7.8	3.8	0.435	1.202 *
180	11/11	144:58	16.1	8	9.83	8.96	7.86		-0.03	92.83	13.1	8.1	2.7	0.584	0.929
181	11/11	217:18	15.5	11	9.84	9.10	8.12		-0.02	93.62	13.5	8.1	2.4	0.559	0.776
182	11/11	249:38	13.5	271	9.83	9.32	8.23		-0.02	92.91	24.2	7.7	6.7	0.482	1.135 *
183	11/11	321:58	11.9	252	9.82	9.44	8.58		-0.01	94.33	27.8	6.2	11.4	0.420	1.280 *
184	11/11	354:18	10.5	357	9.78	9.50	8.28		-0.01	92.08	11.7	7.6	2.5	0.364	0.848 V30
185	11/11	426:39	9.7	341	9.78	9.51	8.07		-0.01	90.79	13.8	7.6	4.1	0.333	1.167 V30

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 1

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrs	Ut	Ute	
186	11/11	458:59	10.4	310	9.75	9.46	7.82		-0.01	89.48	17.0	7.7	9.3	0.360	2.255	V30
187	11/11	531:19	10.0	323	9.00	9.25	7.35		-0.04	87.91	15.6	7.7	7.6	0.351	1.949	V30
188	11/11	603:39	9.5	343	9.69	9.07	7.16		-0.06	87.81	13.9	8.1	2.3	0.331	0.707	V30
189	11/11	635:59	7.2	349	9.58	8.64	6.92		-0.17	88.93	15.3	7.7	4.7	0.248	1.143	V20
190	11/11	708:19	8.5	1	9.48	8.39	6.94		-0.13	90.59	13.3	7.5	1.8	0.298	0.481	V 5
191	11/11	740:39	10.0	10	9.45	8.70	6.06		-0.07	83.49	16.1	7.6	1.1	0.352	0.261	
192	11/11	812:59	10.7	55	9.55	8.62	6.31		-0.07	85.39	10.4	7.8	1.2	0.380	0.457	
193	11/11	958:39	9.3	41	9.81	8.78	7.12		-0.11	89.36	12.8	7.7	0.7	0.328	0.228	
194	11/11	1030:59	7.5	26	9.79	8.98	7.13		-0.13	88.17	11.5	7.5	0.7	0.261	0.220	
195	11/11	1103:19	5.9	7	9.78	8.78	7.18		-0.27	89.68	13.5	7.0	0.8	0.203	0.194	
196	11/11	1247:59	3.6	357	9.94	7.92	6.68		-1.71	91.85	12.8	6.7	1.5	0.124	0.275	R15
197	11/11	1320:19	1.7	8	9.95	7.92	6.81		-0.01	92.69	13.3	6.2	1.6	0.061	0.185	V11
198	11/11	1352:39	2.6	350	9.97	8.03	7.36		-3.23	95.50	16.5	6.1	2.9	0.089	0.311	V30
199	11/11	1424:59	3.6	349	9.97	8.17	7.49		-1.52	95.45	15.8	6.3	2.6	0.121	0.350	V30
200	11/11	1531:39	6.1	14	9.94	9.03	8.49		-0.20	96.40	11.3	6.8	2.0	0.208	0.525	
201	11/11	1603:59	9.9	20	9.92	9.25	8.49		-0.05	95.00	14.8	7.5	2.1	0.348	0.540	V 2
202	11/11	1636:19	6.6	57	9.94	9.16	8.01		-0.15	92.51	7.3	7.4	2.5	0.226	1.173	V30
203	11/11	1708:39	10.9	4	9.98	9.10	7.73		-0.06	91.11	15.2	7.6	1.6	0.384	0.411	V 3
204	11/11	1740:59	11.4	14	9.98	9.51	7.38		-0.03	86.57	14.7	7.6	1.4	0.402	0.377	V 1
205	11/11	1813:20	9.1	277	9.94	9.03	7.62		-0.09	90.83	17.2	7.3	5.2	0.321	1.058	*
206	11/11	1845:39	9.4	59	9.90	9.63	6.95		-0.02	83.38	15.0	7.4	1.6	0.324	0.409	V 4
207	11/11	1917:59	12.9	12	9.89	9.45	6.37		-0.02	81.13	13.6	7.9	1.4	0.457	0.422	
208	11/11	1950:20	12.2	8	9.93	9.46	6.49		-0.03	81.70	13.5	7.8	1.3	0.432	0.382	
209	11/11	2022:40	12.4	11	9.90	9.49	6.00		-0.03	78.82	15.1	7.8	2.4	0.441	0.636	R15
210	11/11	2055: 0	11.7	6	9.96	9.52	5.87		-0.03	77.96	13.8	7.8	1.2	0.414	0.357	
211	11/11	2127:20	10.6	3	9.97	9.51	6.21		-0.04	79.85	14.1	7.6	1.2	0.371	0.328	
212	11/11	2159:40	12.8	33	9.90	9.34	5.89		-0.03	79.04	14.0	8.1	1.4	0.456	0.454	
213	11/11	2236:20	10.5	53	9.77	8.48	6.27	8.73	-0.11	85.99	10.3	7.8	1.2	0.372	0.448	
214	11/11	2308:40	9.4	347	9.77	7.33	5.33	8.79	-0.26	87.11	19.8	7.7	3.7	0.339	0.689	R 2 V10
215	11/11	2341: 0	8.7	288	9.74	7.95	4.39	7.86	-0.24	78.22	38.2	7.3	10.4	0.311	0.921	*
216	11/12	13:20	9.0	272	9.91	8.22	3.27	7.75	-0.22	71.00	57.3	6.6	10.9	0.322	0.581	*
217	11/12	45:40	8.0	285	9.94	8.25	3.03	7.60	-0.28	69.62	44.0	7.0	10.3	0.288	0.752	*
218	11/12	118: 0	8.1	313	9.93	8.16	3.49	8.33	-0.28	72.37	15.0	7.7	8.8	0.290	2.149	V30
219	11/12	150:20	7.9	301	12.05	7.45	3.36	7.52	-0.73	75.30	27.9	7.3	9.7	0.293	1.097	R14 V30
220	11/12	222:40	8.0	309	9.91	8.24	2.44	7.82	-0.28	66.84	16.9	7.5	9.1	0.286	1.913	V30
221	11/12	255: 0	7.3	320	9.71	8.28	1.94	7.66	-0.30	64.36	16.4	7.7	8.3	0.259	1.829	V30
222	11/12	327:20	6.8	55	9.69	8.15	2.94	7.58	-0.37	69.67	8.8	7.3	1.3	0.239	0.465	
223	11/12	359:40	7.2	57	9.83	7.75	3.25	7.74	-0.42	73.18	12.6	7.2	1.0	0.258	0.252	
224	11/12	432: 0	9.7	46	9.90	8.43	2.66	7.00	-0.17	67.02	10.9	7.7	1.2	0.348	0.429	R 5
225	11/12	504:20	9.6	58	9.87	8.49	2.59	7.32	-0.16	66.39	10.9	7.5	0.9	0.342	0.297	
226	11/12	536:40	8.8	142	9.86	8.33	2.41	7.27	-0.21	66.27	10.9	6.9	1.1	0.314	0.310	*
227	11/12	609: 0	5.7	89	9.85	8.22	2.87	7.48	-0.57	69.01	9.4	6.7	0.8	0.201	0.240	*
228	11/12	641:20	8.3	346	9.87	7.84	3.03	8.13	-0.30	71.57	13.3	7.5	1.4	0.300	0.357	V30
229	11/12	713:41	8.0	321	9.86	8.00	2.22	7.46	-0.31	66.89	17.8	7.5	5.1	0.287	0.956	V30
230	11/12	746: 1	6.7	310	9.86	7.71	3.72	7.98	-0.50	75.85	27.4	7.3	7.7	0.240	0.864	R 2 V30
231	11/12	921:41	4.1	86	9.82	8.13	3.96	7.76	-1.19	75.01	8.8	6.6	0.9	0.141	0.235	*



# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 1

FILE	DATE	TIME	U	RDir	Ts	Tg	Td	Tir	Z/L	RH	B	V	Vrms	Us	Ute	
232	11/12	954:1	4.5	99	9.83	7.89	3.85	7.94	-1.13	75.61	11.9	7.1	1.2	0.154	0.253	*
233	11/12	1026:21	4.7	97	9.83	8.31	3.67	7.54	-0.82	72.61	8.4	6.9	1.0	0.161	0.325	*
234	11/12	1058:41	6.8	90	9.81	8.89	3.72	7.00	-0.23	70.01	12.0	7.1	1.2	0.236	0.311	*
235	11/12	1131:1	6.5	95	9.82	8.55	3.91	7.68	-0.33	72.59	8.4	7.2	3.1	0.228	1.146	R 2 *
236	11/12	1506:1	11.6	342	9.77	8.74	2.06	7.78	-0.09	62.90	11.3	8.2	1.2	0.414	0.471	
237	11/12	1538:21	11.3	345	9.79	7.95	1.63	7.88	-0.15	64.33	12.8	8.2	1.3	0.408	0.430	
238	11/12	1610:41	10.4	353	9.81	7.96	1.49	7.49	-0.18	63.63	13.0	8.0	2.5	0.377	0.777	V30
239	11/12	1643:1	11.6	317	9.82	8.29	1.55	7.47	-0.12	62.48	17.7	7.9	7.4	0.417	1.702	V23
240	11/12	1715:21	14.8	11	9.84	8.04	2.25	7.57	-0.08	66.81	13.6	8.1	1.5	0.543	0.479	
241	11/12	1747:41	14.5	10	9.87	7.82	2.49	7.56	-0.09	69.01	14.1	8.1	1.4	0.533	0.423	
242	11/12	1820:1	13.9	15	9.85	7.33	2.48	7.61	-0.13	71.30	13.5	8.1	1.4	0.509	0.450	
243	11/12	1852:1	15.2	33	9.87	7.80	1.96	7.12	-0.09	66.54	12.4	8.1	1.6	0.559	0.551	
244	11/12	2019:1	13.7	9	9.89	7.72	0.79	7.24	-0.12	61.54	14.1	8.0	1.5	0.502	0.440	
245	11/12	2051:21	12.6	8	9.87	7.67	0.34	7.12	-0.14	59.75	14.8	8.0	1.4	0.460	0.372	V 1
246	11/12	2123:41	11.7	233	9.84	7.31	1.35	7.59	-0.19	65.88	21.6	7.3	8.0	0.426	1.259	*
247	11/12	2156:1	10.1	238	9.83	7.75	1.83	7.24	-0.21	66.16	37.9	6.7	9.0	0.363	0.680	*

## DATA TAPE NO. 2

1	11/12	2239:1	9.8	245	9.71	7.76	1.59	7.22	-0.21	65.00	24.0	6.1	10.0	0.354	1.111	R 5 *
2	11/12	2311:22	8.4	256	9.74	8.43	1.78	7.12	-0.21	62.95	12.1	7.1	4.5	0.299	1.181	*
3	11/12	2343:42	11.4	178	9.75	7.84	1.63	7.60	-0.15	64.84	15.2	7.1	2.1	0.411	0.433	*
4	11/13	16:2	9.7	180	9.80	8.06	1.57	7.22	-0.20	63.57	14.5	6.6	2.2	0.350	0.417	*
5	11/13	48:21	7.8	264	9.79	7.99	1.69	6.99	-0.32	64.40	18.4	7.3	6.1	0.279	1.072	*
6	11/13	120:41	9.7	24	9.77	7.67	1.91	6.04	-0.23	66.91	13.1	8.0	3.3	0.351	0.984	R 5 V 7
7	11/13	153:1	9.8	22	10.08	7.65	2.04	6.28	-0.26	67.64	13.6	8.2	1.1	0.354	0.343	R 2
8	11/13	225:21	9.2	15	9.74	7.79	1.67	7.44	-0.24	65.26	12.9	8.2	1.0	0.333	0.315	V 1
9	11/13	257:41	6.7	334	9.75	7.82	2.46	7.08	-0.47	68.88	17.9	7.4	4.1	0.238	0.716	V30
10	11/13	330:1	6.7	308	9.76	7.55	2.14	7.32	-0.54	68.54	16.8	7.6	9.1	0.238	1.794	V30
11	11/13	402:21	5.3	308	9.76	7.71	1.81	7.88	-0.86	66.28	15.2	7.2	8.6	0.185	1.644	V30
12	11/13	434:41	6.3	293	9.70	7.99	1.66	7.44	-0.50	64.26	20.5	6.7	7.6	0.222	1.051	*
13	11/13	507:1	6.6	276	9.73	8.06	1.39	7.30	-0.44	62.80	25.6	6.6	9.8	0.235	1.048	*
14	11/13	539:21	6.0	323	9.73	7.98	1.37	7.21	-0.50	63.05	23.1	7.4	5.1	0.210	0.706	V30
15	11/13	611:41	5.3	275	9.71	7.69	1.86	6.29	1.83	66.57	15.4	6.4	6.4	0.186	1.002	R 3 *
16	11/13	644:1	4.7	358	9.73	7.31	2.21	7.05	-1.25	70.07	13.0	7.1	1.0	0.166	0.216	R 3
17	11/13	716:21	5.3	36	9.73	7.98	1.73	6.75	-0.75	64.67	18.1	7.2	1.9	0.184	0.319	V12
18	11/13	748:41	7.2	135	9.64	8.06	1.96	6.94	-0.34	65.40	13.7	6.3	1.7	0.257	0.280	R 9 *
19	11/13	1005:1	8.1	11	9.62	8.14	1.63	7.14	-0.25	63.55	12.4	7.4	0.8	0.291	0.235	
20	11/13	1037:21	6.3	335	9.60	7.88	1.94	7.32	-0.69	69.81	14.5	8.0	3.7	0.225	0.896	V30
21	11/13	1109:41	6.9	335	9.62	8.09	1.15	7.22	-0.37	61.55	15.9	8.0	3.7	0.245	0.873	V30
22	11/13	1142:1	8.1	331	9.66	8.26	2.60	7.49	-0.23	67.52	14.3	8.1	5.4	0.288	1.508	V30
23	11/13	1214:21	8.5	337	9.66	8.30	2.66	7.61	-0.21	67.64	15.9	8.2	3.5	0.301	0.907	V30
24	11/13	1417:21	7.0	65	9.58	8.42	2.51	6.68	-0.27	66.36	8.2	7.3	2.1	0.246	0.833	*
25	11/13	1449:41	9.1	72	9.66	8.51	2.73	6.61	-0.16	66.99	8.2	7.5	1.0	0.321	0.451	*
26	11/13	1522:1	8.8	75	9.59	8.55	2.72	6.59	-0.15	66.78	8.4	7.4	0.9	0.310	0.395	*
27	11/13	1554:21	10.5	36	9.56	8.65	2.05	6.42	-0.10	63.25	11.7	8.0	1.1	0.372	0.405	
28	11/13	1626:42	8.7	3	9.74	8.23	2.41	6.13	-0.22	66.72	23.3	7.8	3.2	0.311	0.518	R15 V14

# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 2

FILE	DATE	TIME	U	RDir	Ts	To	Td	Tir	Z/L	RH	B	V	Vrms	U#	U#e	
29	11/13	1659:2	9.4	2	11.58	8.70	2.11	5.27	-0.34	63.28	15.1	7.6	1.8	0.343	0.418	R 3
30	11/13	1731:22	9.6	355	9.66	8.72	2.49	7.30	-0.12	64.90	15.0	7.7	1.8	0.339	0.450	
31	11/13	1803:42	8.6	54	9.65	8.68	2.72	7.10	-0.15	66.17	10.1	7.7	1.0	0.303	0.388	
32	11/13	1836:2	9.9	63	9.64	8.82	3.18	7.29	-0.10	67.74	13.1	7.7	1.0	0.349	0.299	*
33	11/13	1908:22	9.5	63	9.56	8.84	2.23	7.04	-0.10	63.21	13.8	7.7	0.9	0.334	0.256	*
34	11/13	2200:42	11.2	324	9.56	9.17	3.31	7.58	-0.04	66.75	15.2	8.4	7.4	0.396	2.197	V30
35	11/13	2233:2	11.0	316	9.58	9.16	4.08	7.25	-0.04	70.48	17.2	8.3	8.5	0.386	2.201	R 6 V30
36	11/13	2305:22	11.4	316	9.59	9.41	4.10	7.74	-0.02	69.40	30.7	8.6	8.7	0.399	1.322	V30
37	11/13	2337:42	11.9	310	9.64	9.51	4.24	7.97	-0.02	69.64	16.3	9.1	9.2	0.420	2.762	V30
38	11/14	10:2	14.1	7	9.65	9.58	4.81	7.65	-0.01	72.14	20.0	8.9	2.0	0.502	0.493	
39	11/14	42:22	13.1	7	9.63	9.73	5.37	7.83	0.00	74.27	17.4	8.9	1.9	0.458	0.518	
40	11/14	114:42	12.7	15	9.61	9.86	5.49	7.12	0.01	74.21	15.2	8.6	1.8	0.441	0.532	R 2
41	11/14	147:2	12.2	51	9.63	9.95	5.54	7.85	0.02	74.05	13.1	8.6	1.9	0.422	0.623	R 1
42	11/14	219:22	11.4	128	9.61	9.92	5.99	7.74	0.02	76.57	7.9	8.3	1.8	0.390	0.896	*
43	11/14	251:42	11.8	137	9.61	9.79	6.06	7.58	0.01	77.60	7.4	8.3	1.8	0.406	0.995	*
44	11/14	324:2	12.9	140	9.59	9.83	5.97	7.95	0.01	76.87	10.9	8.4	1.9	0.448	0.736	*
45	11/14	356:22	14.4	153	9.60	9.88	5.84	7.94	0.01	75.97	16.4	8.5	2.4	0.506	0.627	*
46	11/14	428:42	14.2	170	9.62	9.88	5.76	7.88	0.01	75.53	16.2	8.4	3.7	0.500	0.949	R 3 *
47	11/14	501:2	14.0	169	9.60	9.96	6.09	7.75	0.02	76.88	14.7	8.4	3.4	0.489	0.944	*
48	11/14	533:22	14.5	13	9.59	9.97	6.32	7.57	0.02	78.09	19.6	9.2	1.8	0.511	0.451	
49	11/14	605:42	13.8	58	9.67	10.05	5.99	7.97	0.02	75.90	16.0	9.0	2.2	0.481	0.622	
50	11/14	638:2	14.4	219	9.69	9.96	6.10	7.99	0.01	76.92	32.6	8.2	6.1	0.507	0.770	*
51	11/14	710:22	13.4	296	9.63	9.98	6.49	7.91	0.02	78.93	47.1	8.0	11.7	0.465	0.994	*
52	11/14	1022:15	12.8	252	9.56	9.92	6.19	7.37	0.02	77.59	16.7	8.9	3.1	0.444	0.821	R 3 *
53	11/14	1054:35	12.3	252	9.42	10.12	6.38	7.10	0.05	77.57	17.6	9.0	3.4	0.419	0.816	R 2 *
54	11/14	1126:55	13.2	277	9.41	10.20	6.50	7.38	0.05	77.81	25.7	9.0	5.5	0.454	0.916	R 1 *
55	11/14	1159:15	16.4	162	9.37	10.23	6.38	7.39	0.03	77.00	13.0	8.5	6.3	0.581	1.976	*
56	11/14	1231:35	12.3	306	9.36	10.22	6.72	7.65	0.06	78.89	44.4	8.9	10.7	0.419	1.003	V30
57	11/14	1303:55	13.3	311	9.37	10.26	7.10	7.60	0.05	80.75	38.1	9.2	9.5	0.457	1.094	V30
58	11/14	1336:16	13.4	338	9.38	10.14	6.92	7.39	0.04	80.44	22.4	9.1	8.3	0.462	1.644	R13 V30
59	11/14	1448:36	13.8	352	9.45	10.27	7.35	7.67	0.05	82.89	29.2	8.2	7.2	0.475	0.975	V30
60	11/14	1520:56	14.1	347	9.49	10.37	7.31	7.83	0.05	81.29	17.0	8.3	6.2	0.486	1.470	V30
61	11/14	1603:56	14.6	354	9.49	10.34	7.30	7.89	0.04	81.47	18.4	8.2	6.3	0.508	1.370	V30
62	11/14	1830:36	17.9	7	9.28	10.45	7.39	7.61	0.04	81.34	11.7	8.1	1.9	0.637	0.687	
63	11/14	1902:56	17.5	5	9.37	10.50	7.19	7.87	0.04	79.97	10.9	8.1	1.6	0.624	0.594	
64	11/14	2105:36	11.9	95	9.26	10.20	7.88	8.15	0.08	85.51	12.7	8.1	2.2	0.398	0.615	*
65	11/14	2137:56	10.5	104	9.46	10.24	7.70	8.35	0.08	84.25	7.8	8.3	2.6	0.349	1.121	*
66	11/14	2210:16	12.2	98	9.41	9.95	7.90	8.43	0.04	87.89	11.2	8.4	2.5	0.416	0.854	*
67	11/14	2242:36	13.2	93	9.38	9.99	7.88	7.99	0.04	86.74	14.5	8.5	2.6	0.455	0.710	R 5 *
68	11/14	2314:56	14.9	61	9.38	9.86	7.91	8.72	0.03	87.69	8.1	8.8	2.5	0.523	1.394	*
69	11/14	2347:16	20.9	17	9.33	9.88	8.23	8.59	0.01	89.49	13.9	9.0	2.6	0.767	0.927	
70	11/15	19:36	21.8	14	9.36	9.87	8.59	8.64	0.01	91.77	20.7	9.1	3.2	0.807	0.787	
71	11/15	51:56	23.8	14	9.41	9.99	8.73	8.60	0.01	91.85	21.0	8.9	3.0	0.893	0.721	
72	11/15	124:16	24.4	6	9.43	10.33	9.00	8.52	0.02	91.47	13.6	8.9	3.3	0.916	1.204	
73	11/15	156:36	23.8	8	9.42	10.56	9.40	8.17	0.02	92.55	13.0	8.8	3.6	0.886	1.358	R 4
74	11/15	228:56	23.6	10	9.46	10.79	9.71	8.51	0.02	93.88	13.7	8.7	3.4	0.880	1.191	

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 2

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	Us	Ute	
75	11/15	301:16	22.2	7	9.46	10.97	9.96	8.52	0.03	93.51	11.8	8.6	3.3	0.817	1.292	
76	11/15	333:36	23.3	5	9.47	11.21	10.21	8.54	0.03	93.60	17.4	8.7	3.4	0.864	0.903	
77	11/15	405:56	25.1	8	9.51	11.39	10.29	8.57	0.03	92.98	11.6	8.8	2.6	0.938	1.096	
78	11/15	438:17	24.9	7	9.48	11.38	9.13	8.27	0.03	86.03	11.7	8.8	3.7	0.932	1.535	R30
79	11/15	510:37	26.2	5	9.53	11.75	10.55	8.60	0.03	92.34	14.6	8.9	3.0	0.985	1.005	
80	11/15	542:57	26.2	7	9.56	11.91	10.48	8.37	0.03	90.97	11.2	8.9	2.8	0.984	1.233	R 3
81	11/15	615:17	26.2	5	9.51	12.00	10.51	8.60	0.03	90.63	10.8	8.9	2.5	0.984	1.132	R15
82	11/15	647:37	26.9	4	9.48	12.29	10.45	8.59	0.03	88.53	10.5	8.9	2.3	1.015	1.050	
83	11/15	719:57	26.9	11	9.50	12.65	10.30	8.58	0.04	85.64	11.1	8.9	2.4	1.011	1.034	
84	11/15	752:17	27.1	5	9.45	12.60	10.19	8.52	0.04	85.24	11.5	9.0	2.3	1.022	0.993	
85	11/15	824:37	26.5	6	9.40	12.85	10.06	8.48	0.04	83.16	10.4	8.9	2.1	0.993	0.959	
86	11/15	856:57	25.3	3	9.35	12.70	10.12	8.45	0.05	84.26	10.0	8.9	2.1	0.938	0.978	
87	11/15	929:17	25.0	2	9.33	12.28	10.42	8.47	0.04	88.38	13.0	9.0	2.9	0.930	1.048	
88	11/15	1001:37	24.4	1	9.33	11.83	10.56	8.52	0.04	91.94	12.3	9.0	2.7	0.905	1.066	
89	11/15	1033:57	9.9	82	10.27	9.44	8.38	8.25	-0.07	93.13	8.6	8.5	3.0	0.347	1.471	R 2 *
90	11/15	1106:17	6.2	128	9.36	7.72	6.81	8.27	-0.40	94.01	14.7	8.8	2.1	0.217	0.512	*
91	11/15	1138:37	7.4	126	9.32	6.82	5.80	8.12	-0.43	93.22	8.6	9.0	2.1	0.265	0.950	*
92	11/15	1210:57	7.9	127	9.26	5.91	4.71	8.13	-0.51	92.00	5.9	9.3	2.2	0.288	1.434	*
93	11/15	1505:38	12.4	324	9.21	5.61	2.67	8.16	-0.22	81.39	21.9	9.6	4.2	0.455	0.954	V14
94	11/15	1534:58	11.8	298	9.17	6.23	1.72	7.76	-0.20	72.82	21.0	9.5	8.1	0.433	1.829	*
95	11/15	1604:18	9.9	326	9.17	6.67	1.29	7.45	-0.25	68.52	14.8	9.9	6.6	0.361	2.176	V30
96	11/15	1820:17	14.1	14	9.16	5.76	2.14	7.02	-0.16	77.54	13.7	9.4	1.3	0.521	0.467	
97	11/15	1852:37	11.6	292	9.13	6.32	1.99	7.44	-0.20	73.82	12.3	9.2	1.3	0.425	0.488	*
98	11/15	1924:56	12.0	247	9.18	7.33	2.27	7.19	-0.13	70.26	12.1	8.8	1.6	0.432	0.566	R 6 *
99	11/15	1957:16	13.5	33	11.13	7.47	2.00	4.61	-0.19	68.23	9.1	9.3	2.2	0.498	1.138	R22
100	11/15	2029:36	14.3	136	9.23	7.26	2.73	7.29	-0.09	72.93	11.0	9.2	1.3	0.523	0.567	*
101	11/15	2101:56	11.0	171	9.22	7.53	2.42	7.09	-0.14	70.88	9.3	8.9	1.5	0.396	0.669	*
102	11/15	2134:17	13.4	213	9.25	7.56	2.15	7.01	-0.09	68.59	19.2	9.1	1.5	0.486	0.347	*
103	11/15	2206:37	8.5	116	9.24	7.76	2.39	6.77	-0.22	68.82	9.1	8.8	1.3	0.385	0.560	*
104	11/15	2324:37	9.9	26	9.23	7.66	3.07	6.52	-0.16	72.74	16.8	8.9	3.1	0.356	0.808	V25
105	11/15	2356:57	8.0	89	9.23	8.10	2.99	7.79	-0.19	70.18	11.6	8.8	1.1	0.282	0.373	*
106	11/16	29:17	10.4	44	9.22	8.30	1.58	6.88	-0.10	62.58	14.0	9.0	2.9	0.370	0.936	V12
107	11/16	101:37	9.3	86	9.23	8.39	0.70	6.77	-0.12	58.38	14.2	8.9	1.1	0.329	0.340	R 6 *
108	11/16	133:57	9.1	86	9.21	8.32	0.12	4.37	-0.14	56.29	12.6	8.9	1.6	0.321	0.529	R27 *
109	11/16	206:17	11.1	302	9.24	8.42	1.21	6.83	-0.08	60.45	24.3	8.9	7.8	0.393	1.443	V29
110	11/16	238:37	10.5	64	9.23	8.34	1.84	6.83	-0.09	63.60	10.9	8.9	1.1	0.374	0.456	*
111	11/16	310:57	10.9	54	9.22	8.30	1.80	6.63	-0.09	63.61	13.0	9.0	1.8	0.387	0.615	V 3
112	11/16	343:17	12.1	333	9.23	7.99	2.20	7.02	-0.09	66.85	23.9	9.0	6.7	0.434	1.298	V23
113	11/16	415:37	11.6	61	9.24	7.52	2.27	6.31	-0.13	69.34	15.9	9.0	1.1	0.418	0.305	*
114	11/16	447:57	11.7	330	9.24	7.76	2.33	5.87	-0.11	68.50	54.4	8.5	6.6	0.420	0.519	V17
115	11/16	520:17	11.8	30	9.25	7.76	2.22	6.65	-0.11	67.95	36.0	8.8	3.0	0.423	0.371	V 2
116	11/16	552:37	10.8	260	9.24	8.01	1.86	6.85	-0.12	65.10	41.7	8.0	9.8	0.384	0.928	*
117	11/16	624:57	11.0	29	9.25	8.15	2.76	7.50	-0.10	68.80	19.7	8.8	2.2	0.392	0.487	V 6
118	11/16	657:17	7.8	291	9.26	7.90	2.42	7.49	-0.24	68.29	27.9	7.8	7.8	0.278	0.989	*
119	11/16	729:37	9.6	360	9.24	7.44	3.06	7.12	-0.20	73.75	20.1	8.7	2.7	0.344	0.570	R 7 V13
120	11/16	1104:57	6.2	297	9.19	6.65	3.61	8.05	-0.68	80.93	24.1	8.3	5.6	0.221	0.795	*

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 2

FILE	DATE	TIME	U	RDic	Ts	Tg	Td	Tir	Z/L	RH	B	V	Vrms	U <sub>1</sub>	U <sub>2</sub>	
121	11/16	1400:58	6.5	125	9.20	7.76	4.58	7.27	-0.36	80.34	23.5	6.9	3.1	0.227	0.332	R19 *
122	11/16	1554:38	8.7	56	9.27	7.52	4.10	7.79	-0.23	78.92	16.9	9.3	0.9	0.313	0.236	
123	11/16	1626:58	7.2	30	9.29	7.61	3.95	7.60	-0.34	77.63	16.2	9.2	0.8	0.254	0.209	
124	11/16	1659:18	5.0	338	9.29	7.75	3.86	7.90	-0.68	76.39	22.1	9.6	0.6	0.174	0.117	
125	11/16	1731:38	6.1	325	9.23	7.87	3.13	7.22	-0.41	71.98	19.7	9.7	1.6	0.213	0.360	R 5 V20
126	11/16	1803:58	6.4	308	9.22	7.98	2.92	7.61	-0.35	70.40	48.9	8.0	3.5	0.221	0.252	V30
127	11/16	1836:18	5.8	313	9.19	8.03	2.69	7.56	-0.41	68.98	14.4	7.7	3.0	0.199	0.707	V30
128	11/16	1908:38	6.5	298	9.18	7.92	2.99	7.72	-0.33	71.02	16.0	7.6	4.9	0.228	1.007	*
129	11/16	1940:58	2.0	338	9.10	7.94	2.77	7.41	-3.98	69.82	16.3	7.3	4.4	0.068	0.606	R 5 V30
130	11/16	2013:18	8.7	60	9.15	8.16	2.59	7.49	-0.15	67.90	12.5	7.8	2.1	0.307	0.639	R 9 *
131	11/16	2045:38	8.3	63	9.11	8.09	3.30	7.66	-0.16	71.75	10.3	7.8	0.9	0.294	0.328	R 1 *
132	11/16	2117:58	8.5	28	9.14	8.07	3.17	7.48	-0.16	71.20	13.1	8.2	0.5	0.300	0.162	
133	11/16	2150:18	6.9	76	9.16	8.15	2.70	7.69	-0.24	68.54	10.0	7.6	0.7	0.242	0.218	*
134	11/16	2222:38	6.4	99	9.18	8.36	3.32	7.42	-0.24	70.57	13.0	7.8	1.2	0.219	0.300	R18 *
135	11/16	2254:58	10.2	57	9.20	8.27	3.60	7.39	-0.09	72.40	10.5	8.7	1.3	0.362	0.564	R 3
136	11/16	2327:18	9.6	56	9.32	8.36	3.44	7.86	-0.11	71.15	12.6	8.6	0.8	0.341	0.288	
137	11/16	2359:38	11.3	73	9.35	8.37	3.81	8.11	-0.08	72.97	16.3	8.6	1.4	0.401	0.377	*
138	11/17	31:58	10.1	42	9.29	8.48	3.46	8.00	-0.09	70.72	12.8	8.7	0.8	0.356	0.263	
139	11/17	104:18	10.8	34	9.26	8.51	3.67	8.11	-0.07	71.58	14.3	8.9	0.8	0.384	0.253	
140	11/17	136:38	9.9	226	9.24	8.87	3.98	7.21	-0.05	71.39	15.0	7.9	2.9	0.346	0.713	R 6 *
141	11/17	208:58	10.7	195	9.34	9.85	4.31	8.30	0.03	68.42	22.4	7.5	2.6	0.363	0.352	*
142	11/17	241:18	10.9	109	9.35	8.98	4.14	8.26	-0.04	71.69	14.1	8.2	1.5	0.384	0.429	*
143	11/17	313:38	10.8	330	9.30	8.28	2.47	8.29	-0.10	66.80	27.7	9.0	3.7	0.386	0.615	V22
144	11/17	345:58	11.0	320	9.19	7.25	3.36	8.25	-0.15	76.35	13.9	8.5	4.3	0.398	1.347	V22
145	11/17	418:19	13.1	9	9.16	7.07	4.16	8.34	-0.11	81.72	12.6	8.8	1.5	0.478	0.550	
146	11/17	450:39	13.7	360	9.20	6.71	5.16	8.27	-0.12	89.87	22.1	9.0	3.0	0.500	0.663	R 2
147	11/17	522:59	14.8	360	9.16	7.27	6.50	8.40	-0.07	94.90	13.0	8.9	3.2	0.539	1.230	
148	11/17	555:19	14.5	16	9.22	8.15	7.61	8.44	-0.04	96.40	14.8	8.5	3.1	0.522	0.983	
149	11/17	627:39	13.1	42	9.21	9.58	9.16	8.51	0.04	97.22	15.3	8.0	3.1	0.452	0.803	
150	11/17	659:59	15.1	22	9.15	9.70	8.82	8.39	0.03	94.29	12.2	8.3	2.5	0.530	0.858	R 9
151	11/17	732:19	16.2	18	9.22	9.41	8.10	7.88	0.01	91.54	9.4	8.3	2.1	0.577	1.012	R 6
152	11/17	804:39	17.0	32	9.12	9.00	6.90	8.37	-0.00	86.68	23.2	8.2	3.4	0.618	0.690	
153	11/17	1324:58	15.6	310	9.13	8.14	2.22	7.77	-0.04	66.25	0.0	0.0	0.0	0.570		
154	11/17	1357:18	14.9	306	-10.87	8.43	1.98	8.04	1.37	63.84	0.0	0.0	0.0	0.319		R 7
155	11/17	1557:59	15.6	4	7.45	8.28	1.85	8.06	0.03	63.91	0.0	0.0	0.0	0.551		
156	11/17	1806:39	14.8	136	9.11	8.32	1.65	7.87	-0.04	62.82	0.0	0.0	0.0	0.537		*
157	11/17	1838:59	15.4	1	9.14	8.37	2.41	7.86	-0.04	66.12	0.0	0.0	0.0	0.559		
158	11/17	1911:19	14.5	359	9.18	8.13	2.04	7.83	-0.05	65.44	0.0	0.0	0.0	0.527		
159	11/17	1943:39	14.7	118	11.32	8.39	2.81	6.74	-0.13	67.94	0.0	0.0	0.0	0.542		R21 *
160	11/17	2015:59	17.3	12	9.92	8.03	3.55	8.24	-0.06	73.34	0.0	0.0	0.0	0.641		R15
161	11/17	2048:19	16.8	0	9.16	7.16	3.04	7.85	-0.07	75.05	0.0	0.0	0.0	0.620		
162	11/17	2120:39	15.2	2	9.16	8.14	3.31	8.12	-0.04	71.53	0.0	0.0	0.0	0.553		
163	11/17	2152:59	15.0	6	9.16	7.35	3.30	8.50	-0.08	75.50	0.0	0.0	0.0	0.548		
164	11/17	2225:19	13.4	346	9.15	8.15	4.21	8.06	-0.05	76.20	0.0	0.0	0.0	0.482		R 4
165	11/17	2257:39	12.6	358	9.16	8.21	3.30	7.69	-0.06	71.15	0.0	0.0	0.0	0.453		R 7
166	11/17	2329:59	12.4	16	9.17	8.58	3.19	8.40	-0.04	68.86	0.0	0.0	0.0	0.441		

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 2

FILE	DATE	TIME	U	RDip	Ts	Tg	Td	Tir	Z/L	RH	B	V	Vrms	Ut	Ute
167	11/18	2:19	15.3	349	9.16	8.33	2.70	7.85	-0.04	67.69	0.0	0.0	0.0	0.556	
168	11/18	34:39	14.9	354	9.15	8.42	2.19	8.08	-0.04	64.86	0.0	0.0	0.0	0.541	
169	11/18	106:59	14.4	348	9.14	8.43	1.47	7.91	-0.04	61.54	0.0	0.0	0.0	0.521	
170	11/18	139:19	14.9	350	9.14	8.29	1.96	7.44	-0.04	64.37	0.0	0.0	0.0	0.542	R 6
171	11/18	211:39	14.7	1	9.13	7.94	1.78	8.28	-0.06	65.05	0.0	0.0	0.0	0.534	
172	11/18	243:58	10.5	37	9.11	8.06	2.39	7.84	-0.10	67.42	0.0	0.0	0.0	0.372	
173	11/18	316:18	13.8	132	9.12	8.33	1.22	7.64	-0.05	60.89	0.0	0.0	0.0	0.498	*
174	11/18	348:38	12.5	43	9.13	8.38	1.33	7.92	-0.06	61.14	0.0	0.0	0.0	0.446	
175	11/18	420:58	13.3	342	9.13	8.58	2.06	8.29	-0.04	63.56	0.0	0.0	0.0	0.477	
176	11/18	453:18	13.4	338	9.10	8.40	3.41	7.57	-0.04	70.83	0.0	0.0	0.0	0.479	R26
177	11/18	525:38	13.7	342	9.13	8.14	4.05	8.52	-0.05	75.42	0.0	0.0	0.0	0.495	
178	11/18	557:58	11.5	150	9.13	6.78	3.99	8.45	-0.17	82.40	0.0	0.0	0.0	0.418	*
179	11/18	630:18	11.6	109	9.16	7.48	3.60	8.13	-0.12	76.41	0.0	0.0	0.0	0.420	*
180	11/18	702:39	14.1	355	9.17	8.07	3.12	8.19	-0.06	70.94	0.0	0.0	0.0	0.509	
181	11/18	734:59	14.0	5	9.12	7.87	2.54	7.43	-0.07	69.04	0.0	0.0	0.0	0.506	R 6
182	11/18	807:19	14.2	357	9.66	8.02	1.72	7.67	-0.08	64.42	0.0	0.0	0.0	0.518	R 3
183	11/18	839:39	14.3	357	9.09	8.19	1.16	7.83	-0.05	61.21	0.0	0.0	0.0	0.516	
184	11/18	911:59	10.3	357	9.08	8.31	1.17	7.75	-0.09	60.76	0.0	0.0	0.0	0.365	
185	11/18	944:19	12.9	326	9.09	8.18	2.09	7.86	-0.06	65.48	0.0	0.0	0.0	0.464	
186	11/18	1016:39	12.7	357	9.07	7.31	1.88	7.95	-0.11	68.42	0.0	0.0	0.0	0.460	
187	11/18	1048:59	10.4	102	9.07	8.07	2.86	7.97	-0.10	69.68	0.0	0.0	0.0	0.369	*
188	11/18	1227:19	7.9	342	9.05	7.60	2.89	7.62	-0.24	72.09	0.0	0.0	0.0	0.282	R 2
189	11/18	1259:39	8.1	352	9.06	7.89	2.87	7.64	-0.19	70.54	0.0	0.0	0.0	0.286	
190	11/18	1331:59	8.5	348	8.93	8.07	2.18	7.38	-0.14	66.36	0.0	0.0	0.0	0.298	
191	11/18	1404:19	8.8	342	8.94	4.00	-2.84	6.01	-0.63	60.99	0.0	0.0	0.0	0.328	R10
192	11/18	1503:39	5.4	90	8.98	8.40	1.46	7.60	-0.29	61.68	0.0	0.0	0.0	0.182	*
193	11/18	1535:59	4.3	130	9.00	8.45	2.37	7.76	-0.46	65.59	0.0	0.0	0.0	0.140	R 7 *
194	11/18	1608:19	5.5	339	8.99	8.54	2.01	8.32	-0.23	63.50	0.0	0.0	0.0	0.185	
195	11/18	1640:39	5.6	315	9.02	8.57	1.51	7.96	-0.23	61.18	0.0	0.0	0.0	0.188	
196	11/18	1827:19	9.6	298	8.99	8.57	2.95	7.94	-0.06	67.76	0.0	0.0	0.0	0.336	R 2 *
197	11/18	1859:39	10.6	317	9.00	8.57	3.14	7.92	-0.05	68.69	0.0	0.0	0.0	0.371	
198	11/18	1931:59	9.8	76	9.02	8.50	3.11	7.91	-0.06	68.86	0.0	0.0	0.0	0.346	*
199	11/18	2004:19	12.5	276	9.01	8.43	3.35	8.06	-0.04	70.40	0.0	0.0	0.0	0.445	*
200	11/18	2036:39	14.6	2	9.02	8.62	4.00	8.23	-0.02	72.72	0.0	0.0	0.0	0.526	
201	11/18	2108:59	14.6	5	9.02	8.75	4.86	8.22	-0.01	76.59	0.0	0.0	0.0	0.523	
202	11/18	2146:40	14.3	99	9.01	8.97	5.56	8.50	-0.00	79.20	0.0	0.0	0.0	0.511	*
203	11/18	2219: 0	14.7	302	9.00	9.05	6.41	8.38	0.01	83.53	0.0	0.0	0.0	0.520	R 5
204	11/18	2251:20	16.7	5	9.01	8.97	6.91	8.12	0.00	86.88	0.0	0.0	0.0	0.598	R 5
205	11/18	2323:40	16.3	279	8.99	8.60	6.87	8.63	-0.01	88.86	0.0	0.0	0.0	0.589	*
206	11/18	2356: 0	20.0	9	9.00	8.34	6.99	8.63	-0.01	91.22	0.0	0.0	0.0	0.745	
207	11/19	28:20	21.6	5	9.92	8.52	7.49	8.57	-0.02	93.27	0.0	0.0	0.0	0.816	R17
208	11/19	100:40	20.7	16	9.33	9.08	8.14	8.72	-0.00	93.84	0.0	0.0	0.0	0.770	R30
209	11/19	133: 0	20.1	16	9.00	9.85	9.09	7.75	0.02	95.02	0.0	0.0	0.0	0.731	R22
210	11/19	205:20	20.6	31	9.00	10.32	9.53	8.84	0.03	94.84	0.0	0.0	0.0	0.748	R 3
211	11/19	237:40	17.4	299	9.02	10.49	9.64	8.90	0.05	94.49	0.0	0.0	0.0	0.612	*
212	11/19	310: 0	16.7	317	9.01	10.50	9.64	8.85	0.06	94.39	0.0	0.0	0.0	0.586	

# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 2

FILE	DATE	TIME	U	RDir	Ts	Tq	Td	Tir	Z/L	RH	B	V	Ums	Ut	Ute	
213	11/19	342:20	18.3	20	9.01	10.47	9.52	8.81	0.05	93.85	0.0	0.0	0.0	0.649		
214	11/19	414:40	16.8	19	9.02	10.37	9.49	8.79	0.05	94.31	0.0	0.0	0.0	0.588		
215	11/19	447: 0	12.4	22	9.00	10.26	9.63	8.77	0.10	95.87	0.0	0.0	0.0	0.411		R 6
216	11/19	519:20	11.7	222	8.98	10.18	9.63	7.92	0.11	96.33	0.0	0.0	0.0	0.386		R 4 *
217	11/19	551:40	11.9	8	8.99	10.25	9.77	8.80	0.11	96.82	0.0	0.0	0.0	0.394		
218	11/19	624: 0	12.6	32	8.96	10.23	9.83	8.79	0.10	97.32	0.0	0.0	0.0	0.421		
219	11/19	656:20	6.7	284	8.96	10.04	9.49	8.82	0.38	96.41	0.0	0.0	0.0	0.188		*
220	11/19	728:40	6.6	304	8.99	9.92	9.37	8.66	0.34	96.40	0.0	0.0	0.0	0.188		R 6
221	11/19	801: 0	10.4	36	8.99	9.86	9.31	8.73	0.11	96.34	0.0	0.0	0.0	0.342		
222	11/19	833:20	11.3	21	8.96	9.54	8.87	8.68	0.07	95.58	0.0	0.0	0.0	0.379		R10
223	11/19	905:40	12.3	25	8.94	8.98	8.26	8.67	0.02	95.26	0.0	0.0	0.0	0.426		
224	11/19	938: 0	11.4	9	8.92	8.39	7.10	8.69	-0.03	91.61	0.0	0.0	0.0	0.400		
225	11/19	1010:20	11.0	15	8.92	8.09	5.16	8.48	-0.06	81.72	0.0	0.0	0.0	0.389		
226	11/19	1042:40	7.8	298	8.92	8.36	3.84	8.39	-0.10	73.15	0.0	0.0	0.0	0.271		*
227	11/19	1115: 0	8.3	297	8.92	8.51	3.19	8.38	-0.08	69.21	0.0	0.0	0.0	0.287		*
228	11/19	1147:20	8.2	307	8.94	8.35	1.69	7.91	-0.11	62.88	0.0	0.0	0.0	0.288		R 7
229	11/19	1532: 1	7.2	22	8.95	8.13	1.99	8.20	-0.19	65.21	0.0	0.0	0.0	0.250		
230	11/19	1604:21	7.4	29	8.93	7.95	2.22	8.33	-0.20	67.13	0.0	0.0	0.0	0.261		
231	11/19	1636:41	8.7	26	8.92	7.86	1.95	8.32	-0.16	66.21	0.0	0.0	0.0	0.307		R22
232	11/19	1709: 1	8.6	29	8.89	7.76	2.14	6.36	-0.17	67.63	0.0	0.0	0.0	0.306		R25
233	11/19	1741:21	8.6	219	8.91	7.81	1.22	8.29	-0.17	63.09	0.0	0.0	0.0	0.304		*

## DATA TAPE NO. 3

1	11/19	2047: 1	9.7	311	8.97	7.34	0.98	7.57	-0.19	63.97	0.0	0.0	0.0	0.346		
2	11/19	2119:20	11.3	53	8.94	7.26	1.22	7.75	-0.14	65.48	0.0	0.0	0.0	0.409		
3	11/19	2151:40	10.6	37	8.89	7.04	1.24	7.59	-0.17	66.61	0.0	0.0	0.0	0.382		
4	11/19	2224: 0	9.9	310	8.89	6.52	1.06	7.83	-0.25	68.14	0.0	0.0	0.0	0.357		
5	11/19	2256:20	4.2	93	8.87	6.60	1.05	6.29	-1.56	67.70	0.0	0.0	0.0	0.145		R 5 *
6	11/19	2328:40	4.3	112	8.88	7.10	1.40	7.77	-1.18	67.03	0.0	0.0	0.0	0.148		*
7	11/20	1: 0	4.6	122	8.92	6.88	0.24	7.35	-1.18	62.61	0.0	0.0	0.0	0.159		*
8	11/20	33:20	4.0	111	8.99	7.30	-0.12	7.39	-1.36	59.26	0.0	0.0	0.0	0.138		*
9	11/20	105:40	4.5	109	9.00	7.23	-1.32	7.23	-1.15	54.59	0.0	0.0	0.0	0.155		*
10	11/20	138: 0	6.4	97	8.98	7.26	-0.66	6.66	-0.50	57.14	0.0	0.0	0.0	0.224		R 4 *
11	11/20	210:20	11.5	16	9.02	7.28	-0.37	7.64	-0.14	58.27	0.0	0.0	0.0	0.417		
12	11/20	242:40	12.2	12	9.03	7.22	-0.28	7.70	-0.13	58.93	0.0	0.0	0.0	0.441		
13	11/20	315: 0	12.3	357	9.03	7.34	0.02	8.08	-0.12	59.72	0.0	0.0	0.0	0.444		
14	11/20	347:20	12.7	359	8.96	7.37	-0.83	7.77	-0.11	56.04	0.0	0.0	0.0	0.461		
15	11/20	419:41	12.7	6	8.98	7.34	-1.48	7.53	-0.11	53.54	0.0	0.0	0.0	0.462		
16	11/20	452: 0	12.0	301	8.94	7.39	0.03	7.30	-0.12	59.56	0.0	0.0	0.0	0.435		R 4
17	11/20	524:21	11.9	313	8.92	6.41	0.57	8.17	-0.18	66.26	0.0	0.0	0.0	0.434		
18	11/20	556:41	13.0	326	8.91	6.39	1.30	8.01	-0.15	69.93	0.0	0.0	0.0	0.474		
19	11/20	629: 1	14.1	339	8.95	6.86	0.69	7.95	-0.10	64.78	0.0	0.0	0.0	0.516		
20	11/20	701:21	13.4	52	8.96	6.95	0.21	7.88	-0.11	62.21	0.0	0.0	0.0	0.489		
21	11/20	733:41	13.2	151	8.87	6.68	-0.64	6.60	-0.13	59.55	0.0	0.0	0.0	0.482		R19 *
22	11/20	806: 1	11.5	183	11.20	6.07	1.19	6.90	-0.37	70.88	0.0	0.0	0.0	0.427		R30 *
23	11/20	838:21	10.2	359	8.89	6.20	0.92	7.56	-0.26	68.91	0.0	0.0	0.0	0.371		R12

# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 3

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrns	U\$	U\$e
24	11/20	910:41	11.0	11	8.88	6.63	0.58	7.73	-0.19	65.28	0.0	0.0	0.0	0.401	
25	11/20	943: 1	8.3	67	8.90	6.94	0.50	7.97	-0.30	63.51	0.0	0.0	0.0	0.300	
26	11/20	1015:21	8.0	8	8.92	6.58	0.81	7.76	-0.38	66.62	0.0	0.0	0.0	0.291	
27	11/20	1047:41	11.5	9	8.92	7.17	-0.00	7.74	-0.14	60.33	0.0	0.0	0.0	0.415	
28	11/20	1120: 1	7.8	292	8.91	7.20	0.71	8.04	-0.30	63.41	0.0	0.0	0.0	0.280	*
29	11/20	1234: 1	8.7	356	8.82	6.47	-0.18	7.49	-0.32	62.47	0.0	0.0	0.0	0.315	R 1
30	11/20	1305:41	9.7	204	8.89	7.33	0.15	7.69	-0.18	60.33	0.0	0.0	0.0	0.348	*
31	11/20	1428:41	5.9	92	8.96	6.82	1.79	7.44	-0.67	70.26	0.0	0.0	0.0	0.209	*
32	11/20	1501: 1	6.9	87	8.90	7.04	1.36	7.58	-0.43	67.13	0.0	0.0	0.0	0.244	*
33	11/20	1533:21	8.1	1	8.93	7.10	0.64	7.48	-0.30	63.50	0.0	0.0	0.0	0.292	
34	11/20	1605:41	8.6	5	8.89	7.09	-0.16	7.54	-0.26	59.95	0.0	0.0	0.0	0.308	
35	11/20	1638: 1	8.3	8	9.42	6.93	0.57	5.63	-0.37	63.94	0.0	0.0	0.0	0.302	R22
36	11/20	1936:41	8.2	265	8.85	7.30	0.17	6.55	-0.26	60.53	0.0	0.0	0.0	0.294	R15 *
37	11/20	2009: 1	5.1	326	8.89	7.02	0.40	7.56	-0.85	62.77	0.0	0.0	0.0	0.179	
38	11/20	2041:21	4.9	323	8.88	6.98	1.14	7.65	-0.95	66.37	0.0	0.0	0.0	0.169	
39	11/20	2113:41	5.8	22	8.93	6.95	0.38	7.35	-0.68	62.93	0.0	0.0	0.0	0.204	
40	11/20	2146: 2	6.3	11	8.93	6.95	-0.18	7.39	-0.56	60.46	0.0	0.0	0.0	0.224	
41	11/20	2218:22	5.3	43	8.91	6.88	0.40	5.74	-0.84	63.34	0.0	0.0	0.0	0.186	R 4
42	11/20	2250:42	6.1	61	8.84	6.94	0.59	7.25	-0.59	63.96	0.0	0.0	0.0	0.214	R 6 *
43	11/20	2323: 2	5.6	75	8.90	6.96	0.10	7.39	-0.71	61.65	0.0	0.0	0.0	0.198	*
44	11/20	2355:22	4.1	52	8.88	6.98	-0.44	7.51	-1.44	59.20	0.0	0.0	0.0	0.141	
45	11/21	27:42	4.2	16	8.89	6.97	-0.45	7.44	-1.37	59.18	0.0	0.0	0.0	0.145	
46	11/21	100: 2	3.5	5	8.90	6.96	-0.44	7.30	-2.10	59.30	0.0	0.0	0.0	0.120	
47	11/21	132:22	3.3	48	8.92	7.04	-0.90	6.56	-2.29	57.03	0.0	0.0	0.0	0.114	R 7
48	11/21	204:42	3.4	62	8.92	6.96	-1.08	7.26	-2.25	56.60	0.0	0.0	0.0	0.117	*
49	11/21	237: 2	3.9	58	8.92	6.94	-0.08	7.40	-1.66	60.92	0.0	0.0	0.0	0.134	
50	11/21	309:22	3.7	59	8.90	6.81	-0.01	7.45	-1.91	61.79	0.0	0.0	0.0	0.129	
51	11/21	341:42	2.9	57	8.89	6.80	-0.15	7.59	-3.34	61.19	0.0	0.0	0.0	0.099	
52	11/21	414: 2	2.2	29	8.88	6.83	0.27	7.29	-5.61	62.96	0.0	0.0	0.0	0.077	
53	11/21	443: 2	1.1	311	8.87	6.56	-0.27	7.31	####	61.68	0.0	0.0	0.0	0.044	R 5
54	11/21	515:22	1.9	238	8.90	6.90	-0.34	7.26	-7.26	59.94	0.0	0.0	0.0	0.068	*
55	11/21	547:42	1.7	250	8.93	6.85	0.23	7.14	-8.76	62.70	0.0	0.0	0.0	0.063	*
56	11/21	620: 2	1.5	2	8.93	6.74	0.77	7.40	####	65.71	0.0	0.0	0.0	0.057	
57	11/21	652:22	1.4	243	8.93	6.91	0.84	7.32	####	65.25	0.0	0.0	0.0	0.053	*
58	11/21	725: 2	1.3	260	8.88	6.68	0.45	6.97	####	64.46	0.0	0.0	0.0	0.050	R10 *
59	11/21	944:22	3.6	352	8.94	6.87	-0.42	7.30	-2.04	59.76	0.0	0.0	0.0	0.125	
60	11/21	1016:42	3.7	21	8.92	6.92	-0.76	7.42	-1.93	58.07	0.0	0.0	0.0	0.126	
61	11/21	1049: 2	5.4	324	8.91	6.94	-1.28	7.58	-0.80	55.84	0.0	0.0	0.0	0.191	
62	11/21	1251:43	7.9	322	8.96	7.42	-0.93	6.86	-0.28	55.42	0.0	0.0	0.0	0.284	R 9
63	11/21	1324: 3	7.3	30	8.22	7.29	-1.33	7.89	-0.22	54.29	0.0	0.0	0.0	0.256	R30
64	11/21	1356:23	8.9	287	10.08	7.42	-1.00	5.04	-0.36	55.12	0.0	0.0	0.0	0.324	R30 *
65	11/21	1428:43	8.5	325	8.86	7.47	-0.79	7.57	-0.22	55.81	0.0	0.0	0.0	0.303	R16
66	11/21	1501: 3	6.6	103	8.89	7.53	-0.31	8.00	-0.38	57.57	0.0	0.0	0.0	0.233	*
67	11/21	1533:23	7.6	96	8.86	7.54	-0.49	8.03	-0.27	56.77	0.0	0.0	0.0	0.270	*
68	11/21	1605:43	7.7	108	8.85	7.46	0.46	8.19	-0.26	61.15	0.0	0.0	0.0	0.275	*
69	11/21	1638: 3	7.2	122	9.38	7.41	-0.21	6.10	-0.42	58.45	0.0	0.0	0.0	0.258	R18 *

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 3

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vres	U8	U8e	
70	11/21	1719:23	7.4	102	8.89	7.53	-0.90	7.88	-0.30	55.15	0.0	0.0	0.0	0.263	*	
71	11/21	1916:43	8.7	95	8.72	7.52	-0.03	7.97	-0.18	58.79	0.0	0.0	0.0	0.309	*	
72	11/21	1949: 3	7.2	111	8.58	7.16	0.63	7.68	-0.31	63.17	0.0	0.0	0.0	0.253	R 8 *	
73	11/21	2021:23	8.8	95	8.54	7.23	0.95	7.47	-0.18	64.34	0.0	0.0	0.0	0.315	R 1 *	
74	11/21	2053:43	9.2	91	8.52	7.26	0.88	7.73	-0.17	63.89	0.0	0.0	0.0	0.326	R 9 *	
75	11/21	2126: 3	9.7	92	8.48	7.37	0.73	7.79	-0.13	62.72	0.0	0.0	0.0	0.346	R 1 *	
76	11/21	2158:23	10.1	92	8.25	7.06	1.32	7.45	-0.12	66.88	0.0	0.0	0.0	0.361	*	
77	11/21	2301:23	9.9	98	8.77	6.91	1.60	8.12	-0.19	68.94	0.0	0.0	0.0	0.357	*	
78	11/21	2333:43	9.7	94	8.71	7.41	1.22	7.62	-0.15	64.85	0.0	0.0	0.0	0.346	*	
79	11/22	6: 3	9.9	94	9.59	7.66	1.47	8.44	-0.21	64.87	0.0	0.0	0.0	0.358	:	
80	11/22	38:23	9.0	102	9.66	7.78	1.69	8.56	-0.24	65.37	0.0	0.0	0.0	0.325	*	
81	11/22	110:43	9.9	98	9.09	7.94	2.20	8.83	-0.21	67.04	0.0	0.0	0.0	0.358	*	
82	11/22	143: 3	9.8	101	9.82	7.88	2.65	8.09	-0.21	69.54	0.0	0.0	0.0	0.353	R 3 *	
83	11/22	215:23	11.4	86	9.94	7.77	2.38	8.72	-0.17	68.67	0.0	0.0	0.0	0.412	*	
84	11/22	247:43	10.9	94	9.92	8.09	2.58	8.92	-0.16	68.17	0.0	0.0	0.0	0.395	:	
85	11/22	320: 3	9.5	103	9.95	8.30	2.36	9.12	-0.19	66.20	0.0	0.0	0.0	0.341	*	
86	11/22	352:23	9.3	106	9.89	8.47	2.47	9.11	-0.18	65.96	0.0	0.0	0.0	0.332	*	
87	11/22	424:43	9.3	108	9.67	8.58	2.68	8.97	-0.14	66.45	0.0	0.0	0.0	0.330	*	
88	11/22	457: 3	9.5	104	9.51	8.59	2.61	8.82	-0.12	66.04	0.0	0.0	0.0	0.335	*	
89	11/22	529:23	10.2	99	9.41	8.59	3.01	8.80	-0.09	68.00	0.0	0.0	0.0	0.360	*	
90	11/22	601:44	9.9	100	9.03	8.65	3.19	8.51	-0.05	68.57	0.0	0.0	0.0	0.346	*	
91	11/22	634: 4	10.2	99	8.79	8.62	3.68	7.59	-0.02	71.10	0.0	0.0	0.0	0.354	R 3 *	
92	11/22	706:24	9.8	97	8.80	8.33	4.05	8.35	-0.05	74.40	0.0	0.0	0.0	0.344	*	
93	11/22	738:44	9.3	104	8.72	8.75	3.30	7.66	-0.01	68.64	0.0	0.0	0.0	0.319	R 4 *	
94	11/29	21:39	7.9	217	7.72	5.22	21.70	7.83	-0.09	292.49	48.6	8.2	10.8	0.276	0.858	*
95	11/29	55:20	7.4	196	8.02	5.43	1.38	8.68	-0.48	75.14	28.6	8.2	9.1	0.266	1.102	*
96	11/29	123:20	7.7	217	8.02	5.09	1.42	8.61	-0.49	77.15	35.6	8.2	10.9	0.280	1.072	R 5 *
97	11/29	155:40	7.6	211	8.54	5.36	1.45	8.45	-0.54	75.90	43.5	8.0	11.2	0.279	0.881	R11 *
98	11/29	228: 0	7.8	204	8.09	5.35	1.16	8.55	-0.45	74.42	35.0	8.0	10.9	0.283	1.074	*
99	11/29	300:20	8.0	200	8.20	5.14	1.09	8.60	-0.47	75.09	44.6	8.0	10.8	0.293	0.848	R10 *
100	11/29	329:20	6.7	197	8.19	4.89	0.48	8.50	-0.75	73.13	35.1	7.9	10.0	0.244	0.905	R 7 *
101	11/29	401:40	6.6	178	7.40	5.58	1.64	8.09	-0.44	75.77	27.9	8.3	5.3	0.232	0.669	*
102	11/29	434: 0	7.0	172	7.40	6.07	1.22	7.79	-0.29	71.08	23.4	8.4	4.2	0.245	0.666	R 4 *
103	11/29	506:20	8.0	144	7.39	6.01	0.88	8.09	-0.23	69.65	16.8	8.7	2.1	0.283	0.487	*
104	11/29	538:40	7.8	141	7.38	6.09	0.50	7.90	-0.23	67.34	12.4	8.8	2.1	0.277	0.664	*
105	11/29	611: 0	8.9	141	7.26	6.10	0.44	7.63	-0.15	67.03	12.7	9.0	2.1	0.316	0.710	*
106	11/29	643:20	8.9	142	7.29	6.14	-0.08	7.19	-0.16	64.40	18.9	9.0	2.4	0.315	0.537	*
107	11/29	715:40	8.9	137	7.23	6.19	0.44	6.89	-0.14	66.63	14.1	9.2	2.5	0.313	0.785	*
108	11/29	748: 0	9.3	135	7.64	6.06	0.14	6.65	-0.19	65.76	12.9	9.3	2.7	0.333	0.917	R 3 *
109	11/29	922: 0	15.5	32	7.36	5.84	-0.53	6.73	-0.06	63.65	23.8	10.0	2.4	0.567	0.546	
110	11/29	954:20	16.8	5	7.36	5.90	0.22	7.12	-0.05	66.88	23.6	9.3	2.2	0.620	0.466	
111	11/29	1026:40	18.4	13	7.35	5.74	-0.43	7.11	-0.04	64.53	17.4	9.4	2.1	0.682	0.637	
112	11/29	1059: 0	17.7	6	7.33	5.77	-0.46	7.02	-0.05	64.23	23.5	9.4	2.0	0.658	0.447	
113	11/29	1131:20	16.9	20	7.35	5.79	-0.08	7.19	-0.05	65.97	20.3	9.2	2.0	0.624	0.505	R 2
114	11/29	1226: 0	14.5	20	7.41	5.88	0.52	7.29	-0.07	68.43	17.5	8.9	2.0	0.529	0.532	R 3
115	11/29	1258:20	15.4	11	7.39	5.86	-0.27	7.03	-0.06	64.74	19.0	9.1	1.8	0.562	0.464	



# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 3

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	U#	Ute
116	11/29	1346:40	14.4	355	7.37	5.78	-1.26	6.89	-0.08	60.55	19.1	9.1	1.9	0.527	0.468
117	11/29	1419:0	14.5	3	7.44	5.68	-1.02	7.00	-0.08	62.05	19.7	9.0	1.6	0.528	0.383
118	11/29	1451:20	14.5	13	7.44	5.52	-1.08	6.81	-0.09	62.49	19.2	8.9	1.7	0.531	0.410
119	11/29	1523:40	14.6	3	7.39	5.46	-1.36	6.67	-0.09	61.44	18.4	9.1	1.6	0.536	0.425
120	11/29	1556:0	14.8	4	7.38	5.47	-2.01	6.81	-0.09	59.57	19.5	9.1	1.6	0.541	0.388
121	11/29	1713:20	8.9	96	7.40	5.60	-1.77	6.95	-0.24	59.05	8.7	8.7	1.9	0.320	0.845 *
122	11/29	1745:40	9.3	98	7.48	5.65	-0.63	7.40	-0.22	64.00	10.1	8.8	2.0	0.335	0.762 *
123	11/29	1818:0	9.0	99	7.40	5.70	-1.38	6.87	-0.22	60.34	7.5	8.8	2.1	0.324	1.083 *
124	11/29	1850:21	8.8	98	7.33	5.85	-2.40	6.66	-0.21	55.41	7.8	8.8	2.1	0.316	1.038 *
125	11/29	1922:41	8.4	103	8.51	5.83	-2.40	6.55	-0.40	55.50	8.9	8.7	2.6	0.305	1.035 R10 *
126	11/29	1955:1	9.4	97	7.22	5.71	-1.92	7.32	-0.19	58.00	7.3	8.9	2.1	0.336	1.141 *
127	11/29	2027:21	9.2	95	7.08	5.72	-2.42	7.15	-0.18	55.85	9.9	8.8	2.1	0.327	0.839 *
128	11/29	2059:41	8.8	100	7.22	5.79	-2.99	7.35	-0.21	53.27	8.0	8.8	2.0	0.315	0.970 *
129	11/29	2132:1	9.5	94	7.29	5.77	-2.83	7.41	-0.19	53.96	11.1	8.9	2.0	0.340	0.716 *
130	11/29	2204:21	10.2	88	7.50	5.84	-2.04	7.58	-0.17	56.96	14.3	8.9	2.0	0.366	0.577 *
131	11/29	2307:21	9.6	92	7.86	5.70	-2.10	7.88	-0.25	57.24	13.7	8.8	1.9	0.346	0.545 *
132	11/29	2339:41	8.5	100	8.28	5.54	-1.37	8.24	-0.39	61.09	8.0	8.8	2.1	0.310	0.965 *
133	11/30	12:1	8.6	100	8.41	6.00	-1.95	8.24	-0.35	56.70	10.2	8.5	2.5	0.310	0.890 R 8 *
134	11/30	44:21	10.2	85	8.38	5.70	-0.18	8.25	-0.26	65.90	22.1	8.9	1.8	0.370	0.847 *
135	11/30	116:41	8.9	107	8.42	5.14	-0.38	8.29	-0.41	67.49	12.1	8.6	2.0	0.327	0.587 R 1 *
136	11/30	149:1	10.1	86	10.38	5.29	-0.31	6.29	-0.49	67.19	14.7	9.0	3.5	0.376	0.934 R25 *
137	11/30	221:21	8.6	93	8.39	5.77	-0.10	8.30	-0.36	65.97	12.0	8.6	1.9	0.313	0.588 *
138	11/30	253:41	11.8	75	8.22	6.20	0.50	7.71	-0.15	66.87	11.9	9.2	1.9	0.426	0.713 *
139	11/30	326:1	11.6	72	7.97	5.84	1.18	7.62	-0.16	72.00	12.4	9.1	1.7	0.419	0.606 *
140	11/30	358:21	9.0	63	7.48	5.93	-0.13	6.94	-0.20	65.09	8.4	8.9	1.6	0.322	0.830 *
141	11/30	430:41	13.0	358	7.26	5.69	0.63	6.61	-0.09	69.95	19.1	9.0	1.8	0.471	0.429 R11
142	11/30	503:1	13.0	3	7.08	5.51	-0.01	7.03	-0.09	67.59	22.3	9.0	1.4	0.470	0.296
143	11/30	535:21	11.3	13	7.02	5.50	0.38	6.71	-0.12	69.58	29.2	8.8	1.5	0.408	0.224
144	11/30	607:41	10.6	8	7.05	5.24	0.10	6.67	-0.16	69.42	22.4	9.0	1.6	0.382	0.320
145	11/30	640:1	10.2	15	7.11	5.55	0.21	6.57	-0.15	68.48	18.4	8.8	1.4	0.365	0.337
146	11/30	712:21	11.8	359	7.19	4.90	0.41	7.16	-0.16	72.70	28.7	9.3	1.7	0.427	0.279
147	11/30	744:41	8.9	4	7.35	3.83	0.27	7.24	-0.42	77.56	19.6	8.8	1.3	0.328	0.272
148	11/30	1026:41	8.1	11	7.17	4.74	-0.48	6.62	-0.37	68.95	16.5	8.5	1.2	0.295	0.284
149	11/30	1059:2	8.9	6	8.10	4.77	0.02	6.60	-0.41	71.35	18.2	8.7	1.2	0.327	0.257 R 3
150	11/30	1219:22	8.6	12	7.01	5.26	-3.42	6.25	-0.26	53.49	20.0	8.5	1.1	0.309	0.210
151	11/30	1345:2	9.3	8	7.06	5.14	-3.82	6.41	-0.24	52.37	18.6	8.6	1.2	0.334	0.264
152	11/30	1524:22	8.9	34	7.06	4.79	-3.54	6.32	-0.30	54.78	7.1	8.9	1.2	0.323	0.709
153	11/30	1556:42	8.4	117	7.26	4.82	-3.15	6.22	-0.36	56.30	9.8	8.4	1.7	0.306	0.580 R 2 *
154	11/30	1629:2	8.9	125	7.59	4.77	-3.11	7.10	-0.37	56.67	8.5	8.3	1.8	0.324	0.689 *
155	11/30	1701:22	8.1	122	7.40	4.71	-3.47	6.90	-0.42	55.39	7.9	8.4	1.7	0.296	0.659 *
156	11/30	1733:42	8.4	124	6.92	4.70	-3.29	6.02	-0.33	56.17	7.7	8.3	1.8	0.304	0.759 *
157	11/30	1806:2	8.8	129	6.50	4.54	-3.77	5.75	-0.27	54.80	10.8	8.2	1.7	0.319	0.517 *
158	11/30	1838:22	9.6	135	6.57	4.53	-3.81	5.82	-0.23	54.71	9.2	8.0	1.7	0.348	0.612 *
159	11/30	1948:42	7.9	120	6.98	4.67	-3.61	6.03	-0.39	54.99	9.8	8.1	1.7	0.287	0.510 *
160	11/30	2021:2	11.0	30	6.93	4.57	-3.74	6.14	-0.20	54.82	16.9	9.6	1.2	0.399	0.335
161	11/30	2053:22	8.8	293	6.97	4.55	-2.25	6.32	-0.32	61.35	23.3	8.6	6.8	0.320	1.152 *

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 3

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	Ux	Uye	
162	11/30	2125:42	9.8	170	7.05	4.67	-2.44	6.39	-0.25	59.95	13.0	7.6	3.8	0.354	0.884	*
163	11/30	2158: 2	8.1	139	7.29	4.64	-2.91	6.55	-0.41	58.00	13.3	7.2	1.8	0.296	0.360	*
164	11/30	2302:22	7.4	128	7.24	4.78	-3.11	6.36	-0.48	56.60	20.6	7.0	1.9	0.266	0.215	*
165	11/30	2334:42	7.9	179	7.30	5.41	-2.84	6.19	-0.32	55.27	20.1	6.5	5.3	0.286	0.591	*
166	12/ 1	7: 2	8.2	205	7.32	5.65	-1.95	6.30	-0.27	58.07	23.9	6.5	8.0	0.293	0.798	R16 *
167	12/ 1	37:42	9.4	226	7.16	5.49	-2.12	6.04	-0.20	58.00	27.6	7.1	10.1	0.336	1.070	R29 *
168	12/ 1	110: 2	11.0	245	7.35	4.74	-0.16	5.67	-0.21	70.53	23.7	7.9	10.4	0.400	1.540	R 4 *
169	12/ 1	142:22	10.1	211	7.41	4.78	-0.11	6.35	-0.25	70.58	31.5	7.2	10.1	0.366	0.945	*
170	12/ 1	214:42	9.5	190	7.34	6.67	-0.62	6.24	-0.09	59.67	25.2	7.0	8.9	0.334	1.015	*
171	12/ 1	247: 2	11.5	184	7.33	5.10	-1.66	6.45	-0.17	61.65	21.5	7.5	8.1	0.416	1.223	*
172	12/ 1	319:22	9.7	212	7.24	5.36	-1.37	6.86	-0.21	61.85	23.9	7.0	10.2	0.348	1.219	*
173	12/ 1	351:42	13.0	117	7.30	5.09	-1.89	6.68	-0.13	60.69	26.9	8.6	4.7	0.475	0.725	*
174	12/ 1	424: 3	11.4	52	7.35	5.22	-2.70	6.71	-0.17	56.63	13.7	9.5	1.4	0.414	0.485	
175	12/ 1	456:22	12.1	28	7.37	5.26	-5.02	6.58	-0.15	47.44	17.9	9.1	1.3	0.439	0.334	
176	12/ 1	528:43	11.7	18	7.34	5.38	-4.17	6.82	-0.15	50.17	18.3	9.5	1.2	0.424	0.321	
177	12/ 1	601: 3	11.4	351	7.18	5.52	-2.42	7.27	-0.14	56.62	20.1	9.9	2.1	0.410	0.562	V14
178	12/ 1	633:23	11.2	336	7.33	5.31	-0.87	7.30	-0.16	64.34	18.3	10.0	4.1	0.405	1.173	V29
179	12/ 1	705:43	11.1	5	7.40	4.11	-0.79	7.40	-0.26	70.40	20.0	9.2	1.6	0.406	0.356	
180	12/ 1	738: 3	12.3	254	7.35	5.26	-1.53	7.29	-0.14	61.54	37.6	9.2	8.4	0.445	1.032	*
181	12/ 1	902:43	11.8	315	7.38	4.77	-1.61	7.29	-0.18	63.32	37.6	9.4	4.8	0.430	0.594	V30
182	12/ 1	1456:23	11.6	8	7.39	3.77	-0.81	7.33	-0.26	71.99	16.7	9.0	1.6	0.427	0.406	
183	12/ 1	2010:22	16.2	49	7.37	2.95	-5.98	7.23	-0.16	51.88	33.3	9.3	1.8	0.609	0.269	R 1
184	12/ 1	2042:42	15.7	20	7.41	2.92	-5.61	7.37	-0.17	53.49	14.8	9.1	2.4	0.588	0.792	V10
185	12/ 1	2115: 2	16.1	351	7.38	2.91	-5.63	7.40	-0.16	53.42	16.7	9.2	2.1	0.603	0.595	V15
186	12/ 1	2147:23	14.6	357	7.32	2.77	-5.56	7.41	-0.20	54.27	13.1	9.2	1.5	0.546	0.542	
187	12/ 1	2219:42	15.0	9	7.22	2.86	-4.55	7.42	-0.18	58.18	15.1	9.2	1.6	0.560	0.511	R 2
188	12/ 1	2252: 3	15.1	7	7.26	2.75	-5.48	7.34	-0.19	54.68	14.8	9.0	1.9	0.563	0.596	R 1
189	12/ 1	2324:23	14.9	3	7.27	2.76	-5.20	7.35	-0.19	55.76	15.3	8.9	1.7	0.558	0.505	
190	12/ 1	2356:43	15.2	7	7.29	2.68	-5.20	7.32	-0.19	56.08	18.8	9.0	2.2	0.569	0.536	R 1
191	12/ 2	29: 3	14.7	24	7.33	2.50	-6.27	7.32	-0.21	52.40	14.8	8.8	1.8	0.552	0.540	
192	12/ 2	101:23	15.3	11	7.36	2.46	-5.42	7.37	-0.19	56.02	17.1	8.9	1.6	0.575	0.441	
193	12/ 2	205:23	15.0	2	7.37	2.46	-5.31	7.38	-0.20	56.52	17.7	9.0	1.6	0.562	0.419	
194	12/ 2	237:43	14.8	2	7.40	2.46	-3.83	7.42	-0.21	63.16	18.9	9.0	1.7	0.554	0.404	
195	12/ 2	310: 3	14.7	6	7.40	2.50	-3.98	7.47	-0.21	62.30	15.8	8.9	1.6	0.552	0.470	
196	12/ 2	342:23	14.9	5	7.37	2.68	-4.87	7.43	-0.20	57.51	16.3	8.9	1.7	0.558	0.476	
197	12/ 2	414:43	14.7	6	7.37	2.80	-4.90	7.26	-0.20	56.93	17.7	8.9	2.0	0.551	0.522	V 5
198	12/ 2	447: 3	16.9	16	7.37	2.79	-5.66	7.29	-0.15	53.78	16.1	9.1	1.8	0.635	0.540	
199	12/ 2	519:23	15.0	3	7.37	2.70	-5.91	7.34	-0.20	53.07	16.8	8.9	1.8	0.561	0.486	V 3
200	12/ 2	551:43	15.3	7	7.35	2.99	-5.60	7.28	-0.17	53.23	15.2	8.9	1.8	0.574	0.539	
201	12/ 2	624: 3	15.7	4	7.34	3.14	-5.01	7.31	-0.16	55.12	17.5	9.0	2.1	0.588	0.564	V 5
202	12/ 2	743: 3	15.9	13	7.37	3.18	-6.11	7.31	-0.15	50.55	16.8	9.0	1.8	0.597	0.520	V 1
203	12/ 2	843:43	16.2	352	7.42	3.11	-5.25	7.29	-0.15	54.22	18.5	9.1	2.0	0.608	0.508	V 4
204	12/ 2	1032: 3	15.1	59	7.31	3.41	-5.63	7.02	-0.16	51.57	12.3	8.7	1.8	0.564	0.654	
205	12/ 2	1104:23	14.3	51	7.32	3.54	-5.19	7.24	-0.18	52.83	12.6	8.6	1.7	0.531	0.627	R 2
206	12/ 2	1136:43	13.8	45	7.21	3.54	-5.42	7.36	-0.19	51.92	13.0	8.6	1.4	0.510	0.490	
207	12/ 2	1209: 3	15.6	22	7.20	3.53	-4.39	7.42	-0.14	56.19	12.8	8.6	1.5	0.583	0.542	

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 3

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	Ut	Ute	
208	12/ 2	1241:23	15.4	5	7.18	3.72	-4.39	7.64	-0.14	55.40	16.3	8.5	1.5	0.572	0.412	
209	12/ 2	1313:43	14.1	322	7.84	3.82	-4.46	7.82	-0.16	54.76	32.7	8.2	4.2	0.520	0.543	V10
210	12/ 2	1729:43	16.3	5	7.25	5.44	-1.07	8.18	-0.07	64.09	12.2	8.5	1.7	0.601	0.630	
211	12/ 2	1802: 4	16.8	293	7.24	5.45	-0.82	7.95	-0.06	63.97	18.3	9.1	5.9	0.621	1.608	*
212	12/ 2	1834:24	17.0	293	7.20	5.22	-0.19	7.88	-0.06	68.08	17.5	9.1	6.2	0.628	1.773	*
213	12/ 2	1906:44	16.2	291	7.18	5.39	-0.49	7.73	-0.07	65.85	18.6	9.0	6.3	0.596	1.656	*
214	12/ 2	1939: 4	16.5	291	7.17	5.76	-1.54	7.22	-0.05	59.40	16.5	9.1	6.2	0.605	1.864	R 8 *
215	12/ 2	2011:24	17.1	293	7.18	5.82	-1.65	8.14	-0.05	58.69	22.8	9.1	6.3	0.631	1.399	*
216	12/ 2	2043:44	16.8	306	6.95	5.68	-1.09	8.32	-0.04	61.76	17.4	9.2	5.4	0.619	1.590	V30
217	12/ 2	2116: 4	18.5	359	6.69	5.47	-2.39	7.88	-0.04	56.92	23.8	9.0	2.7	0.687	0.585	V 6
218	12/ 2	2148:24	19.8	3	6.54	5.36	-3.60	7.63	-0.03	52.43	15.4	9.0	1.9	0.739	0.643	
219	12/ 2	2220:44	19.0	0	6.55	5.25	-4.02	6.81	-0.04	51.22	15.3	8.9	2.1	0.709	0.676	R 4
220	12/ 2	2253: 4	18.7	3	6.49	5.32	-3.81	7.83	-0.03	51.76	12.3	8.9	1.8	0.695	0.728	
221	12/ 2	2325:24	19.3	356	6.33	5.20	-4.38	7.77	-0.03	50.81	13.7	9.2	1.6	0.718	0.612	
222	12/ 3	23:44	18.7	352	6.27	5.23	-3.69	7.85	-0.03	52.58	12.7	9.2	1.7	0.694	0.712	
223	12/ 3	56: 4	18.3	346	6.31	5.17	-3.40	8.20	-0.03	53.93	12.5	9.2	1.6	0.676	0.662	
224	12/ 3	146:44	18.3	348	6.14	5.18	-3.95	8.11	-0.03	51.71	13.4	9.2	1.8	0.678	0.710	R 8
225	12/ 3	219: 4	18.5	348	6.03	5.24	-4.03	8.06	-0.03	51.19	14.8	9.2	2.7	0.684	0.978	R 4
226	12/ 3	251:24	19.4	351	5.90	5.15	-4.26	8.00	-0.02	50.65	13.4	9.3	1.6	0.720	0.633	
227	12/ 3	323:44	18.8	13	5.91	5.17	-3.80	7.91	-0.02	52.37	13.7	8.9	1.7	0.696	0.618	
228	12/ 3	356: 4	18.7	9	6.09	5.18	-3.75	8.11	-0.03	52.52	13.7	8.9	1.7	0.692	0.627	
229	12/ 3	428:24	15.5	58	5.96	5.05	-3.89	7.85	-0.04	52.44	6.8	8.9	2.1	0.563	1.485	R 9
230	12/ 3	500:44	15.2	119	5.83	4.94	-3.81	7.93	-0.04	53.15	6.0	8.7	2.2	0.551	1.671	*
231	12/ 3	533: 4	18.6	111	6.02	4.96	-3.86	7.89	-0.11	52.88	4.7	8.7	2.1	0.376	1.818	*
232	12/ 3	605:24	9.4	107	5.94	4.95	-3.96	7.62	-0.13	52.50	5.8	8.8	2.1	0.334	1.452	*
233	12/ 3	637:44	13.3	40	5.92	5.00	-4.07	7.73	-0.06	51.91	3.8	8.9	1.8	0.480	2.230	
234	12/ 3	710: 4	17.6	5	5.82	5.08	-3.73	7.86	-0.03	52.95	12.9	8.9	1.6	0.649	0.610	R 4
235	12/ 3	747: 4	16.9	14	5.64	5.29	-3.33	7.96	-0.02	53.74	14.0	8.8	1.5	0.615	0.537	
236	12/ 3	846:44	17.2	6	5.63	5.43	-4.20	7.78	-0.01	49.89	13.7	8.7	1.4	0.626	0.519	
237	12/ 3	919: 5	15.2	4	5.62	5.48	-3.33	7.75	-0.01	53.08	14.7	8.6	1.4	0.548	0.460	
238	12/ 3	951:25	14.3	5	5.49	5.54	-2.16	7.68	-0.00	57.65	15.4	8.5	1.3	0.510	0.407	
239	12/ 3	1023:45	14.0	352	5.37	5.47	-1.81	8.42	-0.00	59.40	17.6	8.6	1.7	0.498	0.444	V 6

## DATA TAPE NO. 4

1	12/ 3	1126:45	13.1	359	5.50	5.65	-1.58	8.60	0.00	59.68	13.6	8.4	1.4	0.459	0.461	V 2
2	12/ 3	1159: 5	12.5	358	5.56	5.71	-0.93	8.49	0.00	62.32	17.0	8.4	1.1	0.434	0.275	
3	12/ 3	1231:25	13.0	8	5.63	5.50	-0.04	8.62	-0.01	67.48	15.4	8.4	1.3	0.460	0.371	
4	12/ 3	1303:25	8.2	33	5.58	5.48	0.98	8.24	-0.01	72.75	4.7	8.2	1.5	0.280	1.331	R 5
5	12/ 3	1335:45	12.9	57	5.60	5.45	1.26	7.95	-0.01	74.40	7.2	8.7	1.6	0.455	1.021	
6	12/ 3	1943:45	12.7	325	6.18	5.39	1.18	8.17	-0.05	74.24	26.9	9.2	3.1	0.453	0.560	V24
7	12/ 3	2016: 4	12.2	314	6.27	5.29	1.53	8.43	-0.06	76.70	16.3	9.2	4.5	0.435	1.341	R 3
8	12/ 3	2048:24	12.7	325	5.88	5.47	1.20	7.97	-0.02	73.97	21.5	9.1	4.7	0.450	1.069	V25
9	12/ 3	2120:44	13.4	4	5.58	5.42	1.09	7.90	-0.01	73.69	14.5	8.8	1.3	0.474	0.430	V30
10	12/ 3	2153: 4	13.4	16	5.40	5.64	0.67	8.86	0.01	70.36	15.0	8.7	1.2	0.467	0.365	V22
11	12/ 3	2225:24	13.2	9	5.16	5.64	1.05	7.49	0.03	72.34	12.8	8.7	1.8	0.457	0.598	R14
12	12/ 3	2257:44	12.8	6	5.01	5.20	1.07	7.84	0.01	74.67	15.7	8.8	1.1	0.445	0.316	

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 4

FILE	DATE	TIME	U	RDir	Ts	To	Td	Tir	Z/L	RH	B	V	Vrms	U <sub>0</sub>	U <sub>0e</sub>	
13	12/ 3	2330: 4	13.2	9	4.95	5.43	0.48	7.68	0.03	70.47	13.1	8.8	1.1	0.459	0.356	
14	12/ 4	2:24	13.7	16	4.96	5.33	0.52	8.02	0.02	71.12	16.2	8.8	1.2	0.477	0.317	R 1
15	12/ 4	34:44	12.9	19	4.99	5.36	0.43	7.91	0.02	70.53	15.2	9.1	1.2	0.448	0.357	R 1
16	12/ 4	200:45	13.0	360	5.40	4.81	0.71	8.15	-0.03	74.75	17.8	9.3	1.4	0.464	0.384	
17	12/ 4	233: 5	13.8	7	5.52	4.77	0.63	8.21	-0.04	74.56	16.2	9.3	1.1	0.495	0.353	
18	12/ 4	305:25	11.2	331	5.71	4.92	0.78	8.33	-0.06	74.56	16.6	9.4	3.3	0.396	0.779	V18
19	12/ 4	337:45	10.5	319	5.98	5.21	1.09	8.38	-0.07	74.71	16.6	9.3	4.1	0.370	1.185	V27
20	12/ 4	410: 5	13.3	14	6.03	4.64	1.01	8.34	-0.07	77.31	14.4	9.3	1.4	0.480	0.457	
21	12/ 4	442:25	13.1	14	5.99	4.99	0.83	8.27	-0.05	74.46	16.2	9.2	1.3	0.470	0.393	
22	12/ 4	514:45	13.5	9	5.90	4.91	0.42	8.15	-0.05	72.67	15.1	9.3	1.2	0.485	0.382	
23	12/ 4	547: 5	13.4	351	6.05	5.28	-0.31	7.84	-0.04	67.22	15.8	9.3	1.7	0.479	0.514	V19
24	12/ 4	619:25	13.3	11	6.20	5.01	0.45	8.09	-0.06	72.39	18.4	9.2	1.4	0.480	0.357	V 4
25	12/ 4	651:45	14.1	15	6.07	4.90	0.32	8.21	-0.05	72.21	13.6	9.3	1.3	0.511	0.460	
26	12/ 4	724: 5	9.5	321	5.93	4.78	0.54	8.20	-0.13	74.05	22.9	8.7	4.2	0.335	0.793	V10
27	12/ 4	908: 5	12.6	348	6.15	4.66	0.84	8.11	-0.09	76.25	17.4	9.3	2.8	0.454	0.772	R 5 V 8
28	12/ 4	1504: 5	10.9	5	5.74	5.09	0.18	8.39	-0.06	70.57	16.4	8.9	0.9	0.384	0.240	
29	12/ 4	1536:25	10.3	307	5.72	4.91	0.49	7.81	-0.07	73.04	17.2	9.1	4.6	0.362	1.212	V29
30	12/ 4	1608:45	10.9	344	5.72	5.30	0.39	8.10	-0.04	70.58	30.1	8.9	3.6	0.384	0.549	R 2 V18
31	12/ 4	1716:25	11.7	5	5.82	4.49	0.63	8.31	-0.09	76.00	17.8	9.2	1.1	0.419	0.292	
32	12/ 4	1748:45	11.9	13	5.77	4.84	0.31	7.91	-0.06	72.46	15.6	9.2	1.0	0.426	0.298	
33	12/ 4	1915:26	10.2	355	5.75	4.73	0.63	8.00	-0.09	74.75	14.8	9.1	1.9	0.361	0.576	R 4 V 2
34	12/ 4	1947:46	9.0	251	5.75	4.91	1.16	7.58	-0.10	76.69	31.2	8.2	9.1	0.317	1.108	R 6 *
35	12/ 4	2020: 6	10.1	11	5.82	4.98	0.81	7.91	-0.08	74.44	16.5	8.9	1.2	0.355	0.316	V 4
36	12/ 4	2149:25	10.5	7	5.86	5.00	-0.16	7.68	-0.08	69.27	19.0	9.0	0.9	0.370	0.215	
37	12/ 4	2226:25	10.4	17	5.93	4.90	-0.37	7.74	-0.10	68.71	15.6	9.0	0.8	0.370	0.229	
38	12/ 4	2328: 5	8.7	356	5.80	5.05	-0.66	7.75	-0.11	66.55	27.0	8.7	2.4	0.306	0.381	V 6
39	12/ 5	0:45	8.4	258	5.97	4.88	-0.70	7.65	-0.16	67.13	20.3	8.2	6.1	0.299	1.128	*
40	12/ 5	33:45	8.9	11	6.04	4.42	0.24	7.99	-0.20	74.27	17.5	8.8	1.0	0.319	0.238	
41	12/ 5	106: 5	9.2	13	6.06	4.76	-0.39	7.54	-0.16	69.30	17.1	8.9	0.9	0.327	0.224	
42	12/ 5	138:25	8.9	257	6.06	4.68	-0.51	7.55	-0.18	69.03	35.2	8.4	9.2	0.316	1.030	*
43	12/ 5	210:45	9.5	345	6.10	4.76	0.29	7.96	-0.15	72.78	35.6	8.9	3.1	0.336	0.370	V11
44	12/ 5	243: 5	9.3	26	6.09	4.93	-0.30	7.95	-0.14	68.93	17.5	8.8	1.0	0.330	0.245	
45	12/ 5	315:25	10.0	15	6.12	4.80	-0.42	7.63	-0.13	68.94	17.2	9.0	1.0	0.356	0.256	
46	12/ 5	408:45	10.0	20	6.14	4.38	0.50	8.51	-0.17	75.88	14.9	9.0	1.2	0.358	0.339	
47	12/ 5	441: 5	10.0	358	6.10	4.77	-0.25	7.41	-0.13	69.94	17.6	9.0	1.1	0.357	0.276	R 6
48	12/ 5	513:25	9.4	3	6.09	4.76	-0.62	7.64	-0.15	68.08	17.8	8.9	0.8	0.334	0.203	
49	12/ 5	545:45	10.0	12	6.10	4.42	0.06	7.74	-0.16	73.33	19.7	9.0	0.8	0.358	0.181	
50	12/ 5	618: 5	8.1	10	6.11	4.29	0.29	7.95	-0.27	75.23	18.5	8.7	0.8	0.289	0.171	
51	12/ 5	650:25	8.8	14	6.13	4.29	0.58	8.20	-0.23	76.82	16.7	8.8	1.1	0.314	0.269	
52	12/ 5	1051:26	6.2	9	6.13	4.57	-0.52	7.25	-0.44	69.54	19.4	8.3	0.8	0.215	0.142	
53	12/ 5	1123:46	6.8	6	6.08	4.51	0.74	7.90	-0.35	76.49	16.3	8.4	1.2	0.238	0.266	V 2
54	12/ 5	1550: 6	3.0	304	5.60	4.71	-0.45	7.57	-1.25	69.21	15.4	7.3	3.9	0.100	0.591	R 2 V29
55	12/ 5	1622:26	3.5	13	5.84	4.72	-0.62	7.94	-1.11	68.32	21.3	7.8	0.9	0.118	0.122	V 4
56	12/ 5	1726:25	4.4	351	5.92	4.23	0.48	7.82	-0.97	76.61	26.1	8.3	1.1	0.152	0.129	V30
57	12/ 5	1758:46	4.2	355	5.94	3.96	0.70	8.27	-1.27	79.28	20.5	8.3	1.5	0.144	0.217	R24 V30
58	12/ 5	2046:26	1.3	96	5.98	4.44	-0.19	7.98	####	71.87	31.4	7.2	1.0	0.048	0.045	*

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 4

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	U <sub>z</sub>	U <sub>te</sub>	
59	12/ 5	2118:46	1.2	153	5.97	4.95	-0.02	8.88	-7.80	70.25	26.1	7.0	3.1	0.045	0.174	*
60	12/ 5	2151: 6	2.8	87	5.95	4.87	-0.18	7.85	-1.84	69.81	17.9	7.6	1.7	0.091	0.222	*
61	12/ 5	2223:26	2.0	25	5.89	4.41	0.06	7.80	-4.47	73.35	19.6	8.2	0.6	0.070	0.072	
62	12/ 6	11:26	2.0	237	5.91	4.94	-0.17	8.40	-3.29	69.53	36.3	7.2	6.7	0.066	0.361	*
63	12/ 6	43:46	3.1	264	5.88	4.54	-0.36	8.50	-1.80	70.49	25.9	7.6	7.3	0.102	0.688	*
64	12/ 6	115: 6	3.1	2	5.95	4.10	-0.93	7.91	-2.37	69.74	20.6	8.0	1.8	0.106	0.211	R10 V30
65	12/ 6	213:26	4.5	33	5.87	4.52	-0.04	8.09	-0.75	72.23	19.0	8.3	0.9	0.155	0.145	V 3
66	12/ 6	245:46	5.4	35	5.86	4.60	0.23	8.54	-0.47	73.29	18.0	8.5	1.0	0.187	0.188	
67	12/ 6	318: 6	3.9	68	5.89	4.57	0.31	8.56	-1.02	73.86	9.4	8.4	1.1	0.131	0.366	*
68	12/ 6	403:46	6.2	18	5.93	4.51	0.42	8.54	-0.39	74.77	20.3	8.7	1.1	0.214	0.197	V 3
69	12/ 6	442:26	7.1	16	5.96	4.48	0.76	8.45	-0.30	76.78	19.3	8.9	1.0	0.249	0.200	R 5
70	12/ 6	514:46	7.6	22	5.98	4.58	1.01	8.60	-0.24	77.60	18.9	9.0	0.9	0.268	0.205	
71	12/ 6	547: 6	8.0	9	5.98	4.66	1.33	8.45	-0.19	78.88	20.1	9.1	1.0	0.284	0.201	
72	12/ 6	619:27	8.4	10	5.92	4.95	1.18	8.58	-0.13	76.57	15.7	9.2	1.1	0.295	0.315	V 4
73	12/ 6	651:47	9.3	10	5.91	5.11	1.42	8.65	-0.09	77.08	17.8	9.3	0.9	0.325	0.241	
74	12/ 6	724: 7	8.5	332	5.87	5.39	1.71	8.59	-0.06	77.18	33.2	9.2	2.6	0.295	0.356	R14 V14
75	12/ 6	852: 7	11.8	6	5.86	5.53	2.35	8.74	-0.02	79.98	13.4	9.4	0.9	0.416	0.315	V13
76	12/ 6	924:27	11.8	2	5.85	5.72	2.75	8.81	-0.00	81.20	13.6	9.4	0.8	0.415	0.298	
77	12/ 6	956:47	9.6	331	5.80	6.05	3.03	8.95	0.04	80.95	22.6	9.1	4.8	0.323	0.906	V16
78	12/ 6	1102:27	13.0	2	5.74	6.36	3.95	8.97	0.04	84.54	15.4	9.6	1.2	0.445	0.362	V 1
79	12/ 6	1134:47	13.0	9	5.71	6.42	4.58	8.96	0.05	88.00	16.3	9.6	1.3	0.443	0.345	
80	12/ 6	1207: 7	13.4	3	5.71	6.57	5.03	8.95	0.06	89.86	15.8	9.7	1.5	0.456	0.435	
81	12/ 6	1239:27	13.3	5	5.70	6.74	5.43	8.98	0.07	91.34	32.7	9.4	1.4	0.450	0.185	
82	12/ 6	1313: 7	13.0	18	7.19	6.90	5.82	8.01	-0.01	92.88	13.6	9.2	1.8	0.461	0.650	R 6
83	12/ 6	1539:47	12.1	210	5.60	7.75	6.87	9.05	0.18	94.14	50.9	7.8	10.7	0.390	0.620	*
84	12/ 6	1612: 7	11.4	314	5.60	7.86	7.01	8.99	0.21	94.33	20.0	9.0	2.0	0.358	0.354	V30
85	12/ 6	1752:47	13.0	12	5.61	8.10	7.60	9.12	0.17	96.64	15.8	9.2	3.9	0.421	0.930	
86	12/ 6	1825: 7	13.2	12	5.62	8.17	7.70	9.12	0.17	96.80	16.7	9.2	4.2	0.429	0.953	
87	12/ 6	1857:27	13.6	3	5.61	8.26	7.76	9.10	0.17	96.68	14.8	9.3	3.7	0.444	0.975	
88	12/ 6	1929:47	12.5	11	5.60	8.19	7.33	8.74	0.20	94.34	26.0	9.1	3.6	0.398	0.499	R17 V11
89	12/ 6	2002: 7	12.8	341	5.60	8.37	7.42	8.91	0.20	93.71	31.8	9.2	3.3	0.410	0.385	R 1 V22
90	12/ 6	2034:28	14.5	13	5.61	8.51	7.61	8.89	0.15	94.03	13.0	9.3	1.2	0.478	0.363	
91	12/ 6	2106:47	12.2	319	5.62	8.56	7.37	8.91	0.23	92.26	21.5	9.1	4.0	0.383	0.650	V15
92	12/ 6	2139: 7	13.7	9	5.62	8.72	7.42	9.06	0.19	91.53	13.8	9.2	1.1	0.444	0.312	
93	12/ 6	2211:28	14.6	9	5.62	8.88	7.47	9.10	0.17	90.89	13.1	9.3	1.3	0.477	0.378	
94	12/ 6	2240: 8	14.4	10	5.86	8.14	5.42	9.10	0.12	82.94	12.9	9.3	2.3	0.484	0.719	R 8 V19
95	12/ 6	2312:27	14.9	9	6.36	9.00	7.68	8.69	0.13	91.44	46.0	9.3	3.5	0.499	0.309	R14 V30
96	12/ 7	30:28	16.4	11	5.62	9.06	7.92	9.08	0.14	92.52	11.9	9.4	1.3	0.550	0.462	
97	12/ 7	102:48	17.6	15	5.62	9.17	8.03	9.09	0.12	92.58	12.5	9.5	1.5	0.602	0.500	
98	12/ 7	223:28	16.6	10	5.61	9.14	8.21	9.12	0.14	93.89	11.0	9.0	2.0	0.560	0.737	
99	12/ 7	255:48	16.6	11	5.63	9.10	8.22	9.14	0.14	94.27	13.0	9.0	2.1	0.558	0.638	
100	12/ 7	427: 8	16.6	7	5.63	9.04	8.28	9.10	0.13	94.97	10.8	7.8	2.5	0.560	0.811	
101	12/ 7	511: 8	16.7	14	5.63	9.10	8.40	9.25	0.13	95.40	11.0	7.9	2.9	0.565	0.917	
102	12/ 7	543:27	16.1	12	5.62	9.13	8.48	9.31	0.15	95.65	12.9	7.9	2.8	0.540	0.739	
103	12/ 7	615:47	15.8	16	5.64	9.09	8.47	9.30	0.15	95.87	15.0	7.8	2.7	0.525	0.597	
104	12/ 7	648: 7	15.4	22	5.66	9.11	8.52	9.31	0.16	96.04	15.3	7.8	2.9	0.510	0.617	

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 4

FILE	DATE	TIME	U	RD1r	Ts	Tq	Td	Tir	Z/L	RH	B	V	Vrms	U8	U8e	
105	12/ 7	720:27	15.0	26	5.66	9.10	8.53	9.46	0.17	96.23	12.2	7.8	2.9	0.493	0.766	
106	12/ 7	844:47	10.0	11	5.85	7.89	7.31	9.19	0.26	96.08	11.8	7.2	1.2	0.306	0.274	
107	12/ 7	917: 7	9.7	14	5.89	7.57	6.82	9.08	0.24	95.01	9.9	7.2	1.0	0.298	0.267	
108	12/ 7	949:27	10.0	18	5.91	7.43	6.55	9.08	0.20	94.15	11.5	7.2	1.1	0.312	0.253	
109	12/ 7	1021:47	11.2	14	5.94	7.25	6.04	9.05	0.13	92.04	12.7	7.4	1.1	0.364	0.257	
110	12/ 7	1054: 7	11.9	2	5.95	7.22	6.08	9.13	0.11	92.43	17.5	7.5	1.8	0.393	0.337	V 2
111	12/ 7	1214:28	11.6	10	6.00	7.26	5.49	9.16	0.11	88.49	13.6	7.9	1.1	0.382	0.272	
112	12/ 7	1246:48	12.2	8	5.99	7.25	4.92	9.09	0.10	85.13	13.7	7.9	1.2	0.405	0.303	
113	12/ 7	1500: 8	12.6	15	5.97	7.38	2.76	8.69	0.09	72.47	10.6	8.0	1.1	0.423	0.382	
114	12/ 7	1550:28	10.4	214	5.79	7.44	3.37	8.83	0.17	75.39	19.4	6.6	9.3	0.332	1.153	R 4 *
115	12/ 7	1741: 8	9.4	353	6.04	7.25	3.85	8.85	0.16	78.96	13.5	7.6	0.9	0.297	0.203	V 4
116	12/ 7	1813:28	9.4	8	6.08	7.19	4.09	8.09	0.15	80.67	13.7	7.6	0.9	0.300	0.196	
117	12/ 7	1845:48	9.3	7	6.07	7.21	4.24	8.08	0.16	81.42	33.2	7.8	0.9	0.297	0.086	
118	12/ 7	1918: 8	8.4	32	6.07	7.25	4.38	7.62	0.21	82.02	9.2	7.9	1.8	0.259	0.558	R 4
119	12/ 7	1950:28	6.8	103	6.09	7.36	4.50	8.94	0.38	82.09	10.6	7.5	1.2	0.191	0.267	*
120	12/ 7	2022:48	9.1	359	6.09	7.42	4.90	8.78	0.20	84.04	15.3	8.3	1.3	0.284	0.258	V 8
121	12/ 7	2055: 8	9.8	10	6.09	7.48	5.22	8.98	0.18	85.56	17.3	8.3	1.1	0.310	0.207	
122	12/ 7	2128:28	8.8	4	6.09	7.52	5.41	8.28	0.23	86.44	15.9	8.2	1.0	0.271	0.197	
123	12/ 7	2200:48	9.4	7	6.11	7.58	5.44	8.46	0.21	86.30	16.4	8.3	1.1	0.292	0.217	
124	12/ 7	2233: 8	9.5	8	6.08	7.64	5.54	7.85	0.22	86.55	16.4	8.3	1.7	0.295	0.328	R 5
125	12/ 7	2305:28	10.4	7	6.09	7.73	5.73	9.15	0.18	87.15	15.7	8.5	1.2	0.330	0.258	
126	12/ 7	2337:48	8.9	263	6.08	7.79	5.89	8.89	0.28	87.79	25.5	7.9	6.2	0.267	0.667	*
127	12/ 8	52: 8	10.2	0	6.08	7.83	6.36	9.11	0.21	90.41	16.3	8.5	1.2	0.320	0.238	
128	12/ 8	117:48	10.3	4	9.29	6.96	4.94	8.70	-0.21	86.98	46.1	8.4	2.9	0.371	0.259	R14
129	12/ 8	142:49	11.0	10	7.29	7.90	6.46	8.62	0.07	90.62	46.3	8.4	2.7	0.370	0.222	R30
130	12/ 8	215: 8	10.8	15	6.03	7.99	6.65	8.71	0.20	91.23	20.0	8.4	3.0	0.341	0.485	R17
131	12/ 8	247:28	10.8	3	6.05	8.00	6.71	8.49	0.21	91.53	16.2	8.5	1.3	0.341	0.254	
132	12/ 8	319:48	9.7	267	6.06	8.03	6.69	8.58	0.27	91.24	35.1	7.7	7.0	0.294	0.550	*
133	12/ 8	352: 8	10.8	160	6.07	8.06	6.60	8.77	0.21	90.47	31.4	7.6	7.7	0.340	0.668	*
134	12/ 8	424:29	11.5	13	6.05	8.11	6.85	7.29	0.19	91.77	18.7	8.6	2.2	0.367	0.392	R 8
135	12/ 8	456:49	12.4	17	6.05	8.15	6.81	8.81	0.16	91.26	15.5	8.7	1.4	0.404	0.321	
136	12/ 8	529: 9	13.0	15	6.06	8.23	6.79	8.67	0.15	90.64	15.6	8.8	1.4	0.426	0.330	
137	12/ 8	601:29	12.9	9	6.05	8.28	6.78	8.58	0.15	90.28	16.3	8.8	1.4	0.422	0.310	
138	12/ 8	633:49	13.1	11	6.06	8.41	6.69	8.75	0.15	88.95	15.0	8.8	1.4	0.429	0.339	
139	12/ 8	706: 9	13.2	14	6.06	8.40	6.56	8.91	0.15	88.16	14.3	8.8	1.4	0.433	0.365	
140	12/ 8	845:49	14.2	11	6.02	8.55	5.88	8.38	0.13	83.30	15.8	8.8	1.5	0.472	0.348	
141	12/ 8	918: 9	14.3	12	6.02	8.51	5.24	8.31	0.13	79.91	14.1	8.8	1.4	0.478	0.383	
142	12/ 8	950:29	14.6	4	6.02	8.53	4.33	8.35	0.12	74.89	15.0	8.8	1.5	0.488	0.388	
143	12/ 8	1056:49	15.0	15	5.96	8.48	3.54	8.55	0.11	71.10	91.3	8.7	1.7	0.506	0.072	V 5
144	12/ 8	1140:49	12.8	316	5.97	8.72	3.75	8.86	0.18	70.97	29.1	8.4	6.4	0.411	0.752	V30
145	12/ 8	1213: 9	13.6	311	5.94	8.89	3.44	8.80	0.16	68.66	30.6	8.5	5.9	0.445	0.685	V24
146	12/ 8	1245:29	15.7	3	5.92	8.79	3.75	8.75	0.12	70.61	14.9	8.9	1.6	0.530	0.435	
147	12/ 8	1317:49	14.9	359	5.90	8.94	3.25	8.67	0.14	67.54	12.4	8.8	1.5	0.498	0.465	
148	12/ 8	1438: 9	15.6	8	5.92	8.85	3.21	8.70	0.12	67.74	13.3	8.8	1.4	0.527	0.407	
149	12/ 8	1510:29	13.7	325	5.94	8.81	3.58	8.78	0.16	69.68	22.9	8.6	3.0	0.450	0.472	R 1 V10
150	12/ 8	1726: 9	14.5	9	6.12	8.47	4.95	9.05	0.12	78.51	13.1	8.8	1.4	0.487	0.401	

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 4

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	Ut	Ute	
151	12/ 8	1758:29	13.6	14	6.15	8.37	5.23	9.11	0.13	80.61	14.8	8.8	1.4	0.452	0.358	
152	12/ 8	1830:49	13.3	10	5.43	8.25	5.55	9.08	0.18	83.10	13.9	8.8	1.4	0.432	0.359	
153	12/ 8	1903: 9	13.5	17	5.60	8.16	5.80	9.05	0.16	85.08	16.4	8.9	1.4	0.441	0.305	
154	12/ 8	2102:30	13.0	7	5.82	7.91	6.28	8.83	0.14	89.41	13.6	8.9	1.2	0.427	0.337	
155	12/ 8	2134:50	13.1	7	5.88	7.83	6.31	8.73	0.13	90.10	15.5	8.9	1.2	0.434	0.299	
156	12/ 8	2207:10	13.8	13	5.91	7.81	6.17	8.84	0.11	89.38	138.0	8.9	1.8	0.462	0.051	
157	12/ 8	2239:30	13.9	12	5.90	7.79	6.07	8.94	0.11	88.88	16.8	9.2	1.9	0.466	0.467	R 2
158	12/ 8	2311:50	13.6	8	5.90	7.72	5.98	9.11	0.11	88.79	16.0	9.2	1.4	0.453	0.342	
159	12/ 8	2344:10	12.9	184	5.95	7.61	5.78	9.18	0.11	88.19	42.3	8.0	9.2	0.428	0.723	*
160	12/ 9	16:30	12.0	328	5.98	7.59	5.84	9.18	0.13	88.71	18.0	9.1	2.6	0.395	0.543	V12
161	12/ 9	216: 8	14.4	8	6.00	7.44	5.76	9.14	0.08	89.43	15.5	9.3	1.5	0.492	0.406	
162	12/ 9	248:28	15.0	11	6.06	7.32	5.51	9.22	0.06	88.30	15.5	9.4	1.4	0.516	0.407	
163	12/ 9	425:48	14.0	10	6.02	7.51	6.42	9.27	0.09	92.82	17.3	9.4	2.1	0.474	0.515	R 1 V30
164	12/ 9	510:48	15.2	11	6.08	7.50	6.44	9.11	0.07	93.02	16.5	9.5	1.8	0.524	0.480	
165	12/ 9	543:28	14.3	13	6.11	7.57	6.52	9.15	0.08	93.05	16.4	9.3	1.7	0.487	0.450	
166	12/ 9	615:48	14.1	3	6.10	7.65	6.45	9.19	0.09	92.12	28.4	9.0	1.7	0.479	0.238	
167	12/ 9	648: 8	14.7	10	6.11	7.72	6.59	9.26	0.08	92.57	14.9	9.0	2.0	0.499	0.554	
168	12/ 9	720:28	13.5	288	6.32	7.31	4.79	9.10	0.06	84.07	37.7	8.7	7.0	0.463	0.750	R12 *
169	12/ 9	752:48	13.8	259	6.06	7.80	7.11	9.30	0.11	95.35	29.3	8.0	9.4	0.463	1.110	R10 *
170	12/ 9	1242:49	14.0	4	6.49	7.40	6.87	9.14	0.06	96.43	16.1	8.4	2.9	0.479	0.702	
171	12/ 9	1315: 8	12.8	5	5.73	7.33	6.81	9.14	0.12	96.54	15.2	8.2	2.7	0.424	0.613	R10 V 7
172	12/ 9	1426:48	10.2	10	6.35	7.59	7.01	9.31	0.16	96.17	10.8	8.0	3.0	0.326	0.898	V30
173	12/ 9	1459: 9	9.0	82	5.99	7.72	7.13	9.31	0.29	96.06	9.6	7.7	2.2	0.271	0.624	*
174	12/ 9	1531:28	9.9	6	5.74	7.76	7.25	9.30	0.27	96.61	17.2	7.7	1.4	0.300	0.227	
175	12/ 9	1603:29	9.0	1	7.17	7.27	7.28	9.28	0.05	100.05	22.5	7.6	2.8	0.299	0.414	R 3
176	12/ 9	1724:49	7.3	14	5.90	7.73	7.16	9.27	0.53	96.16	15.9	7.7	2.6	0.195	0.389	
177	12/ 9	1757: 9	7.6	144	5.95	7.66	7.06	9.38	0.44	95.95	14.1	7.3	3.1	0.211	0.477	*
178	12/ 9	1829:29	7.5	10	6.00	7.63	7.27	9.30	0.43	97.55	13.0	7.6	2.0	0.211	0.368	
179	12/ 9	1901:49	6.8	6	6.07	7.62	7.18	9.30	0.54	97.05	16.8	7.5	3.5	0.181	0.472	
180	12/ 9	1934: 9	6.9	11	6.07	7.62	7.18	8.90	0.51	97.00	28.4	7.5	4.4	0.187	0.350	R 6
181	12/ 9	2006:29	5.7	349	6.12	7.43	6.91	9.33	0.74	96.47	22.9	7.6	3.7	0.138	0.344	V16
182	12/ 9	2038:49	6.0	13	6.14	7.16	6.65	9.19	0.49	96.62	14.8	7.4	2.9	0.159	0.430	
183	12/ 9	2111: 9	5.9	16	6.19	6.91	6.40	9.16	0.37	96.52	14.0	7.4	2.6	0.165	0.436	
184	12/ 9	2143:29	5.5	15	6.23	6.55	6.03	9.02	0.24	96.42	27.8	7.4	2.4	0.159	0.210	
185	12/ 9	2215:49	4.1	12	6.22	6.33	5.82	8.53	0.30	96.48	30.7	7.2	3.3	0.111	0.241	R 5
186	12/ 9	2248: 9	3.5	16	6.20	6.20	5.68	8.96	0.27	96.48	20.4	7.1	2.7	0.095	0.282	
187	12/ 9	2320:29	3.9	27	6.20	6.13	5.65	8.96	0.15	96.76	17.6	7.2	1.7	0.111	0.240	
188	12/ 9	2352:49	2.9	273	6.21	6.12	5.58	8.96	0.28	96.30	18.8	6.2	5.9	0.075	0.545	*
189	12/10	25: 9	3.2	336	6.24	6.04	5.53	8.95	0.03	96.58	27.7	7.1	4.5	0.094	0.455	V15
190	12/10	57:29	4.0	8	6.25	6.12	5.64	9.05	0.09	96.74	17.0	7.3	3.0	0.116	0.468	
191	12/10	230:29	3.1	19	6.28	6.05	5.56	9.11	0.00	96.71	18.8	6.9	1.5	0.090	0.229	
192	12/10	302:49	2.8	33	6.27	6.00	5.54	9.07	-0.07	96.87	17.9	6.9	2.1	0.084	0.328	
193	12/10	335: 9	0.3	8	6.28	6.01	5.54	9.15	-3.77	96.78	24.9	6.2	3.0	0.012	0.188	V30
194	12/10	407:29	2.0	43	6.31	6.02	5.55	9.14	-0.18	96.74	20.7	6.5	1.2	0.059	0.143	V10
195	12/10	510: 9	1.6	112	6.22	6.08	5.53	8.99	0.56	96.25	14.1	6.9	0.8	0.039	0.093	*
196	12/10	542:29	3.6	138	6.20	6.10	5.55	9.11	0.15	96.28	11.8	7.3	0.9	0.101	0.193	*

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 4

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	U <sub>z</sub>	U <sub>te</sub>	
197	12/10	614:49	4.6	163	6.19	6.15	5.58	9.10	0.12	96.13	19.1	7.4	1.9	0.136	0.268	*
198	12/10	647: 9	5.6	110	6.19	6.16	5.60	9.09	0.08	96.19	14.3	7.6	1.6	0.172	0.331	*
199	12/10	719:30	6.2	5	6.21	6.16	5.63	9.11	0.05	96.45	18.7	7.9	0.8	0.198	0.132	R 1
200	12/10	848:29	7.3	18	5.73	6.31	5.68	9.24	0.10	95.73	18.3	8.5	1.1	0.224	0.187	
201	12/10	920:50	8.8	13	5.91	6.42	5.91	9.27	0.11	96.56	16.7	8.8	1.3	0.286	0.276	
202	12/10	953:10	9.6	5	6.03	6.34	5.69	9.21	0.06	95.59	22.6	9.0	1.6	0.318	0.272	
203	12/10	1025:30	11.4	1	6.11	6.23	5.34	9.24	0.03	94.04	19.9	9.4	1.6	0.392	0.371	
204	12/10	1057:50	11.8	1	6.14	6.58	5.93	9.26	0.05	95.64	22.3	9.4	2.3	0.399	0.453	
205	12/10	1202:10	8.7	259	6.21	7.61	7.14	9.47	0.25	96.81	262.6	8.8	9.8	0.266	0.116	*
206	12/10	1234:30	9.8	24	6.21	8.68	8.28	9.54	0.34	97.34	22.5	8.9	2.5	0.289	0.349	
207	12/10	1306:50	9.4	10	6.22	8.90	8.48	9.55	0.42	97.18	18.4	8.8	2.8	0.267	0.437	
208	12/10	1546:30	8.2	236	6.24	8.72	8.15	9.50	0.54	96.24	26.6	7.8	10.1	0.222	0.855	*
209	12/10	1706:50	12.9	5	4.95	6.62	6.01	8.96	0.12	95.85	23.2	9.6	2.9	0.428	0.518	
210	12/10	1739:10	16.3	2	4.89	6.17	5.42	9.11	0.06	94.94	22.9	10.1	2.9	0.568	0.615	
211	12/10	1811:30	17.6	10	6.88	5.49	4.58	8.97	-0.03	93.82	21.9	10.3	3.0	0.649	0.777	
212	12/10	1843:50	17.5	13	4.41	5.05	3.72	8.86	0.03	91.10	43.1	9.9	2.3	0.626	0.279	
213	12/10	1916:10	16.2	7	4.53	5.19	3.16	8.73	0.03	86.71	19.8	9.4	1.9	0.572	0.449	
214	12/10	1948:30	15.6	182	5.15	5.40	2.68	8.81	0.01	82.60	27.8	8.6	6.4	0.552	0.984	R23 *
215	12/10	2036:50	15.5	12	4.71	5.92	3.42	8.39	0.05	83.94	17.1	9.3	1.8	0.540	0.477	
216	12/10	2109:10	15.4	11	4.72	6.33	2.95	8.74	0.07	78.96	19.9	9.3	1.9	0.530	0.410	
217	12/10	2141:30	14.5	7	4.82	6.47	2.99	8.41	0.08	78.43	21.9	9.2	1.8	0.496	0.341	
218	12/10	2213:50	15.0	15	4.71	6.68	2.65	8.88	0.09	75.50	17.2	9.3	1.8	0.512	0.442	R 5
219	12/10	2307:30	14.9	10	4.76	6.75	2.08	9.05	0.09	72.14	17.5	9.3	1.8	0.508	0.425	
220	12/10	2339:50	12.9	157	4.86	6.98	2.69	9.10	0.14	74.13	23.2	7.8	7.6	0.424	1.009	*
221	12/11	12:10	12.1	102	4.98	6.72	3.38	9.05	0.13	79.24	23.2	8.5	4.7	0.398	0.789	*
222	12/11	44:31	14.9	10	4.84	6.20	3.63	8.68	0.07	83.63	17.5	9.3	1.9	0.512	0.462	
223	12/11	122:31	14.2	32	4.81	6.49	2.74	8.27	0.09	76.93	17.9	9.5	1.6	0.480	0.395	
224	12/11	154:51	13.5	19	4.82	6.66	3.79	9.02	0.11	81.91	27.7	9.5	1.5	0.451	0.237	
225	12/11	227:11	14.4	18	5.02	6.38	4.15	8.91	0.07	85.62	19.2	9.2	1.7	0.491	0.394	
226	12/11	259:31	13.0	15	5.06	6.38	4.18	8.70	0.09	85.79	14.6	8.6	1.6	0.437	0.425	
227	12/11	331:51	12.6	13	5.04	6.58	4.01	9.03	0.11	83.66	24.5	8.6	1.5	0.419	0.225	
228	12/11	404:11	12.7	13	5.09	6.35	4.27	9.10	0.09	86.52	17.6	9.0	1.6	0.426	0.351	
229	12/11	436:31	10.7	304	5.23	6.52	2.44	8.74	0.13	75.17	22.0	9.1	6.7	0.348	1.172	R17 V26
230	12/11	502:11	11.5	293	5.11	6.44	-0.43	8.82	0.10	61.49	40.9	9.2	7.4	0.380	0.722	R15 *
231	12/11	534:31	10.8	297	5.03	6.79	3.27	8.77	0.17	78.28	19.2	9.1	6.5	0.343	1.227	*
232	12/11	606:51	11.6	287	4.99	6.77	3.41	8.70	0.15	79.16	26.0	9.1	7.1	0.378	1.018	*
233	12/11	639:11	12.3	280	4.98	6.86	2.66	8.55	0.13	74.60	30.5	9.0	7.7	0.404	0.944	*
234	12/11	711:31	12.2	280	5.00	6.78	2.96	8.74	0.13	76.61	28.4	9.0	7.8	0.401	1.030	*
235	12/11	922:31	14.6	148	5.02	6.86	3.16	8.47	0.09	77.32	15.7	8.6	2.4	0.498	0.552	R 4 *
236	12/11	954:51	14.2	144	4.97	6.89	3.08	8.23	0.10	76.69	15.9	8.5	2.2	0.480	0.484	*
237	12/11	1027:11	13.6	142	5.03	6.96	3.13	8.47	0.11	76.61	15.6	8.4	2.6	0.453	0.562	*
238	12/11	1059:31	9.6	121	4.96	6.97	2.64	8.28	0.25	73.94	10.0	8.9	4.5	0.294	1.303	*
239	12/11	1131:51	12.9	21	5.10	7.05	2.86	8.33	0.12	74.69	9.6	9.3	1.9	0.427	0.770	
240	12/11	1204:11	14.1	4	5.14	7.07	3.17	8.47	0.10	76.23	18.0	9.2	1.7	0.473	0.395	
241	12/11	1236:32	14.3	26	5.12	7.25	2.78	8.25	0.11	73.28	16.3	9.4	1.7	0.488	0.447	
242	12/11	1308:52	15.9	50	5.19	7.20	3.11	8.38	0.08	75.19	19.3	9.7	1.8	0.549	0.427	



# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 4

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	Ut	Ute
243	12/11	1341:12	14.8	45	5.19	7.27	2.99	8.53	0.10	74.27	18.3	9.6	1.7	0.502	0.481
244	12/11	1413:32	15.2	42	5.11	7.36	2.71	9.25	0.10	72.38	17.6	9.7	1.6	0.517	0.421
245	12/11	1445:32	13.8	42	5.21	7.35	3.07	9.98	0.12	74.27	17.6	9.6	1.6	0.461	0.381

## DATA TAPE NO. 5

1	12/11	1521:37	12.5	34	5.30	7.42	2.80	9.94	0.14	72.49	18.5	9.4	1.5	0.407	0.335
2	12/11	1553:57	10.6	8	5.38	7.35	2.94	9.97	0.19	73.57	18.7	8.8	1.4	0.336	0.250
3	12/11	1741:17	7.2	355	5.50	7.20	3.30	10.01	0.44	76.27	22.1	9.1	0.8	0.201	0.119
4	12/11	1813:37	6.8	348	5.51	7.16	3.54	10.09	0.70	77.73	20.1	9.0	0.8	0.149	0.104
5	12/11	1845:57	6.5	339	5.59	7.25	3.52	10.29	0.57	77.19	18.4	9.0	1.5	0.169	0.231
6	12/11	1918:17	7.1	50	5.64	7.32	3.85	10.23	0.46	78.63	21.5	8.6	1.5	0.194	0.188
7	12/11	2000:58	8.8	64	5.54	7.43	3.89	10.17	0.30	78.29	22.0	8.6	1.1	0.262	0.150
8	12/11	2034:18	8.4	61	5.52	7.53	4.46	10.08	0.36	80.87	23.1	8.6	1.1	0.245	0.140
9	12/11	2107:38	8.1	57	5.60	7.59	4.83	10.35	0.40	82.67	23.0	8.5	1.0	0.232	0.124
10	12/11	2140:58	7.9	51	5.55	7.57	5.47	10.09	0.44	86.51	18.4	8.6	1.0	0.222	0.148
11	12/11	2214:18	7.6	43	5.57	7.61	5.79	10.61	0.51	88.24	19.5	8.7	0.9	0.206	0.136
12	12/11	2257:17	8.2	46	5.77	7.74	5.97	10.51	0.40	88.52	18.3	8.7	1.0	0.233	0.155
13	12/11	2329:37	7.4	40	5.79	7.75	6.16	10.35	0.53	89.67	17.9	8.7	0.9	0.198	0.136
14	12/12	5:17	7.6	38	5.81	7.72	6.39	10.19	0.47	91.26	19.0	8.8	0.9	0.211	0.134
15	12/12	37:37	7.3	35	5.71	7.69	6.37	10.23	0.55	91.33	17.8	8.8	0.8	0.195	0.134
16	12/12	109:57	8.7	38	5.62	7.66	6.48	10.06	0.37	92.24	18.0	9.0	0.9	0.251	0.168
17	12/12	142:17	7.8	32	5.70	7.68	6.43	9.96	0.45	91.80	16.2	8.9	0.8	0.219	0.159
18	12/12	214:37	8.6	31	5.77	7.68	6.37	10.00	0.34	91.39	17.4	9.1	0.9	0.253	0.173
19	12/12	246:57	9.3	30	5.98	7.70	6.20	10.77	0.26	90.22	17.0	9.1	1.0	0.282	0.202
20	12/12	319:17	9.4	25	6.03	7.70	6.30	10.23	0.25	90.86	16.7	9.2	1.0	0.287	0.214
21	12/12	351:37	9.8	24	6.08	7.83	5.86	10.28	0.23	87.36	16.9	9.3	1.0	0.303	0.223
22	12/12	423:57	9.8	22	6.12	7.99	5.58	10.24	0.24	84.77	17.0	9.3	1.0	0.303	0.227
23	12/12	525:17	12.2	25	6.23	8.29	4.72	10.69	0.15	78.26	16.5	9.5	1.2	0.397	0.310
24	12/12	557:38	12.5	26	6.22	8.37	4.58	11.04	0.15	77.02	16.3	9.5	1.3	0.408	0.321
25	12/12	629:58	12.8	22	6.37	8.48	4.51	10.82	0.14	76.08	16.8	9.6	1.2	0.420	0.304
26	12/12	702:18	14.0	23	6.81	8.62	4.63	11.48	0.09	76.03	15.3	9.7	1.3	0.474	0.387
27	12/12	849:38	15.0	22	7.32	8.93	5.17	11.64	0.07	77.25	13.5	9.2	1.3	0.515	0.434
28	12/12	921:58	12.0	13	7.18	8.98	5.36	11.66	0.14	78.05	15.2	8.9	3.5	0.392	0.894
29	12/12	954:18	16.5	22	7.27	9.12	5.22	11.86	0.07	76.56	10.5	9.2	1.8	0.573	0.797
30	12/12	1026:38	16.1	25	7.20	9.14	5.33	11.90	0.07	77.04	14.1	9.2	1.5	0.558	0.483
31	12/12	1058:58	16.2	24	6.95	9.18	5.37	11.83	0.08	77.10	19.6	9.2	1.9	0.559	0.426
32	12/12	1209:18	16.7	24	7.12	9.32	6.17	12.18	0.08	80.68	13.9	9.3	1.5	0.577	0.474
33	12/12	1241:38	16.3	23	7.22	9.09	6.70	12.20	0.07	84.99	14.9	9.3	1.8	0.563	0.538
34	12/12	1313:58	16.8	21	7.29	8.97	7.07	12.28	0.06	87.93	14.4	9.4	1.7	0.586	0.567
35	12/12	1518:18	17.8	24	7.39	9.21	8.17	12.51	0.06	93.17	13.6	9.4	2.0	0.627	0.684
36	12/12	1550:38	17.4	26	7.55	9.46	8.61	12.66	0.07	94.43	13.7	9.3	1.9	0.609	0.634
37	12/12	1622:58	17.1	29	7.60	9.73	8.99	12.79	0.08	95.19	14.1	9.3	2.6	0.594	0.836
38	12/12	1731:38	18.1	36	7.68	10.25	9.58	13.33	0.08	95.65	14.4	9.3	2.5	0.633	0.777
39	12/12	1803:58	18.7	41	7.73	10.52	9.80	15.06	0.08	95.34	14.8	9.4	2.6	0.657	0.810
40	12/12	1836:18	18.6	44	7.71	10.53	9.80	16.10	0.08	95.20	15.4	9.4	2.5	0.651	0.727
41	12/12	1908:38	18.9	47	7.67	10.60	9.83	17.01	0.08	95.00	17.3	9.4	2.3	0.663	0.616

# THE BDM CORPORATION

## SUMMARY OF MET DATA FOR STREX DATA TAPE NO. 5

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	U <sub>8</sub>	U <sub>8e</sub>	
42	12/12	1957:58	18.5	44	7.72	10.53	9.72	28.18	0.08	94.73	16.0	9.5	2.2	0.647	0.635	R 4
43	12/12	2030:18	19.0	45	7.88	10.69	9.69	26.75	0.08	93.52	15.5	9.5	2.4	0.667	0.702	
44	12/12	2102:38	18.2	45	7.91	10.77	9.67	26.02	0.09	92.92	14.3	9.4	2.0	0.634	0.642	
45	12/12	2134:59	17.3	45	7.99	10.69	9.75	25.59	0.09	93.92	14.5	9.4	2.0	0.599	0.607	
46	12/12	2207:19	17.1	43	7.98	10.69	9.80	25.28	0.10	94.26	17.5	9.4	2.3	0.590	0.590	
47	12/12	2239:39	16.9	42	8.01	10.60	9.87	24.66	0.10	95.25	18.0	9.4	3.0	0.582	0.931	R 7
48	12/12	2311:59	18.0	47	8.13	10.72	9.96	25.17	0.08	95.06	15.5	9.5	2.3	0.627	0.688	
49	12/12	2344:19	18.2	47	8.22	10.75	9.91	25.24	0.08	94.58	21.1	9.6	2.3	0.635	0.499	
50	12/13	17:38	17.4	47	8.14	10.59	9.79		0.09	94.80	15.3	9.5	2.2	0.605	0.656	
51	12/13	49:58	15.7	30	7.86	10.47	9.78		0.12	95.49	24.2	9.4	4.8	0.533	0.845	R17
52	12/13	149:59	14.2	13	8.13	10.63	9.64		0.14	93.61	23.0	9.0	3.6	0.471	0.604	
53	12/13	222:19	13.1	12	8.16	10.78	10.12		0.18	95.65	15.2	8.7	2.0	0.424	0.458	
54	12/13	254:39	10.7	10	8.17	10.75	9.97		0.28	94.90	15.4	8.4	1.5	0.327	0.301	
55	12/13	326:59	10.8	8	8.19	10.64	9.91		0.27	95.26	17.7	8.4	1.8	0.330	0.315	
56	12/13	359:19	12.4	14	8.26	10.35	9.67		0.16	95.54	17.9	8.7	3.1	0.403	0.607	
57	12/13	431:39	12.0	20	8.35	9.90	9.15		0.13	95.14	16.6	8.7	2.8	0.392	0.615	R 3
58	12/13	509:39	12.0	19	8.44	9.45	7.99		0.09	90.60	16.2	8.7	1.5	0.400	0.353	
59	12/13	541:59	10.5	12	8.49	9.28	6.68		0.08	83.79	17.9	8.5	1.4	0.349	0.277	
60	12/13	614:19	10.8	1	8.53	8.87	5.28		0.03	78.19	20.2	8.6	1.3	0.369	0.256	
61	12/13	646:39	10.9	7	8.55	8.69	4.37		0.01	74.29	18.7	8.6	1.2	0.375	0.283	
62	12/13	718:59	10.0	8	8.57	8.54	4.20		-0.01	74.17	21.0	8.5	1.2	0.346	0.258	
63	12/13	854:39	9.5	5	8.63	8.61	3.74		-0.01	71.43	16.5	8.4	1.1	0.326	0.292	
64	12/13	926:59	9.4	8	8.69	8.71	3.75		-0.01	71.04	16.6	8.4	1.1	0.325	0.291	
65	12/13	959:19	9.2	21	8.68	8.84	3.97		0.01	71.51	20.4	8.3	1.2	0.311	0.236	
66	12/13	1031:39	9.8	22	8.68	8.88	3.99		0.01	71.38	16.8	8.4	1.2	0.334	0.283	
67	12/13	1103:59	9.0	352	8.65	9.02	4.16		0.04	71.60	18.4	8.4	1.3	0.300	0.269	V 4
68	12/13	1224:39	10.8	72	8.51	9.29	4.90		0.07	74.05	12.2	8.8	1.4	0.361	0.461	*
69	12/13	1346:39	10.9	47	8.67	9.41	5.93		0.07	78.86	17.7	8.9	1.1	0.363	0.255	
70	12/13	1418:59	10.2	45	8.65	9.45	6.34		0.09	80.88	18.0	8.9	1.0	0.335	0.224	
71	12/13	1451:19	11.6	49	8.57	9.51	6.67		0.08	82.47	17.8	9.0	1.2	0.388	0.283	
72	12/13	1523:39	12.2	48	8.48	9.55	6.82		0.08	83.10	16.8	9.1	1.3	0.410	0.320	
73	12/13	1555:59	13.2	48	8.50	9.67	7.21		0.07	84.67	17.9	9.2	1.4	0.448	0.338	
74	12/13	1750:59	15.8	48	9.04	10.09	8.26		0.05	88.42	16.9	9.5	1.6	0.551	0.455	
75	12/13	1823:20	16.2	50	8.92	9.99	8.48		0.04	90.30	17.1	9.6	1.7	0.570	0.493	
76	12/13	1855:40	16.8	48	8.81	9.83	8.68		0.04	92.57	17.5	9.7	2.0	0.592	0.562	
77	12/13	1948:40	17.2	48	8.80	9.98	8.97		0.04	93.45	16.6	9.7	2.0	0.609	0.611	
78	12/13	2021:0	18.1	50	8.76	10.14	9.24		0.05	94.16	16.6	9.7	2.3	0.641	0.684	
79	12/13	2053:20	18.5	51	8.73	10.30	9.49		0.05	94.67	32.8	9.7	2.2	0.657	0.339	
80	12/13	2125:40	18.6	53	8.68	10.47	9.72		0.05	95.13	18.9	9.7	2.2	0.661	0.580	
81	12/13	2158:0	19.5	53	8.53	10.75	9.98		0.06	95.04	28.0	9.8	2.3	0.695	0.400	
82	12/13	2253:20	19.0	59	8.57	11.20	10.32		0.07	94.35	16.4	9.4	2.2	0.670	0.618	
83	12/13	2325:40	18.9	63	8.86	11.37	10.42		0.07	93.89	14.3	9.4	2.2	0.665	0.722	*
84	12/13	2358:0	19.4	63	8.84	11.40	10.43		0.07	93.76	31.6	9.2	2.3	0.688	0.335	*
85	12/14	47:40	18.3	31	8.82	11.32	10.52		0.08	94.80	18.9	8.7	2.5	0.640	0.564	
86	12/14	200:0	18.8	18	8.75	11.60	10.88		0.08	95.39	15.5	8.6	2.6	0.657	0.683	
87	12/14	232:20	18.7	8	8.75	11.75	11.04		0.09	95.45	13.3	8.6	2.8	0.652	0.846	

# THE BDM CORPORATION

## SUMMARY OF NET DATA FOR STREX DATA TAPE NO. 5

FILE	DATE	TIME	U	RDir	Ts	Ta	Td	Tir	Z/L	RH	B	V	Vrms	Us	Uke
88	12/14	304:40	17.5	8	8.76	11.78	11.07		0.10	95.39	13.9	8.5	2.4	0.604	0.673
89	12/14	337: 0	17.0	14	8.77	11.78	11.09		0.11	95.50	11.8	8.4	2.3	0.583	0.750
90	12/14	409:20	15.8	259	8.79	11.92	11.12		0.14	94.83	28.9	7.8	9.9	0.529	1.128 *
91	12/14	441:40	16.6	68	8.78	12.07	11.27		0.13	94.89	18.6	8.3	5.0	0.563	0.976 *
92	12/14	514: 0	17.0	7	8.77	12.23	11.29		0.13	94.82	17.7	8.4	2.0	0.578	0.422
93	12/14	546:20	15.8	4	8.77	12.05	11.19		0.14	94.46	15.0	8.4	2.1	0.527	0.513
94	12/14	618:40	15.7	5	8.77	11.93	11.25		0.14	95.55	16.4	8.4	3.3	0.524	0.732
95	12/14	651: 0	15.5	4	8.77	11.89	11.25		0.14	95.83	14.7	8.4	3.6	0.519	0.888
96	12/14	723:20	13.4	35	8.76	11.87	11.25		0.20	95.96	7.6	8.4	3.4	0.428	1.516
97	12/14	854:41	15.0	7	8.74	11.84	11.26		0.15	96.22	13.8	8.1	3.3	0.496	0.814
98	12/14	927: 1	15.0	13	8.75	11.79	11.21		0.15	96.23	15.1	8.1	3.6	0.496	0.816
99	12/14	959:21	10.9	25	8.76	11.69	11.07		0.31	95.95	6.7	7.9	2.7	0.330	1.154

## APPENDIX C

## TIMES OF PROBABLE RADIO INTERFERENCE

NO.	DATE	TIME START	TIME END	NO.	DATE	TIME START	TIME END
1	11/ 5	1604	1711	47	11/13	148	150
2	11/ 5	1926	2013	48	11/13	540	545
3	11/ 5	2202	2211	49	11/13	641	646
4	11/ 6	121	139	50	11/13	716	722
5	11/ 6	500	514	51	11/13	743	837
6	11/ 6	746	918	52	11/13	916	917
7	11/ 6	1134	1236	53	11/13	927	928
8	11/ 6	1731	1756	54	11/13	1219	1224
9	11/ 7	538	541	55	11/13	1238	1252
10	11/ 7	920	949	56	11/13	1301	1309
11	11/ 7	1158	1201	57	11/13	1512	1632
12	11/ 7	1422	1532	58	11/13	1929	1944
13	11/ 7	1804	1807	59	11/13	2009	2015
14	11/ 7	1905	1907	60	11/13	2217	2223
15	11/ 7	2008	2020	61	11/14	113	113
16	11/ 7	2217	2224	62	11/14	422	425
17	11/ 8	121	130	63	11/14	735	815
18	11/ 8	217	225	64	11/14	1003	1006
19	11/ 8	721	905	65	11/14	1053	1058
20	11/ 8	953	1002	66	11/14	1323	1413
21	11/ 8	1133	1150	67	11/14	1624	1800
22	11/ 8	1242	1246	68	11/14	1924	1957
23	11/ 8	1726	1756	69	11/14	2213	2218
24	11/ 8	2001	2012	70	11/15	125	131
25	11/ 9	815	853	71	11/15	407	440
26	11/ 9	1234	1336	72	11/15	540	600
27	11/ 9	1911	1915	73	11/15	1022	1024
28	11/10	724	820	74	11/15	1221	1244
29	11/10	851	935	75	11/15	1322	1340
30	11/10	1117	1200	76	11/15	1606	1741
31	11/10	1835	2049	77	11/15	1919	1949
32	11/11	821	916	78	11/15	2216	2240
33	11/11	1132	1233	79	11/16	56	131
34	11/11	1423	1450	80	11/16	723	805
35	11/11	2006	2021	81	11/16	1115	1248
36	11/11	2307	2310	82	11/16	1342	1415
37	11/12	126	140	83	11/16	1720	1725
38	11/12	419	424	84	11/16	1922	1926
39	11/12	744	845	85	11/16	1939	1940
40	11/12	1114	1115	86	11/16	2004	2017
41	11/12	1141	1149	87	11/16	2205	2223
42	11/12	1202	1208	88	11/17	115	121
43	11/12	1244	1404	89	11/17	420	423
44	11/12	1905	1931	90	11/17	645	654
45	11/12	2208	2214	91	11/17	718	724
46	11/13	107	112	92	11/17	808	813

# THE BDM CORPORATION

TIMES OF PROBABLE RADIO INTERFERENCE DURING STEEX							
NO.	DATE	TIME START	TIME END	NO.	DATE	TIME START	TIME END
93	11/17	1053	1056	139	11/21	1819	1823
94	11/17	1122	1123	140	11/21	1920	1928
95	11/17	1151	1236	141	11/21	2020	2024
96	11/17	1337	1344	142	11/21	2045	2057
97	11/17	1401	1414	143	11/21	2202	2231
98	11/17	1622	1625	144	11/22	112	116
99	11/17	1923	2001	145	11/22	607	510
100	11/17	2209	2213	146	11/22	722	726
101	11/17	2237	2244	147	11/22	748	844
102	11/18	108	115	148	11/29	109	114
103	11/18	426	452	149	11/29	126	137
104	11/18	725	731	150	11/29	232	242
105	11/18	804	807	151	11/29	313	320
106	11/18	1110	1159	152	11/29	412	416
107	11/18	1354	1421	153	11/29	718	721
108	11/18	1520	1527	154	11/29	753	840
109	11/18	1648	1759	155	11/29	1129	1138
110	11/18	2214	2226	156	11/29	1215	1213
111	11/19	11	125	157	11/29	1310	1313
112	11/19	140	143	158	11/29	1603	1543
113	11/19	419	425	159	11/29	1911	1921
114	11/19	510	514	160	11/29	2225	2230
115	11/19	719	725	161	11/29	2358	5
116	11/19	803	813	162	11/30	116	144
117	11/19	1110	1204	163	11/30	420	432
118	11/19	1244	1410	164	11/30	755	832
119	11/19	1615	1704	165	11/30	1056	1141
120	11/19	1746	1853	166	11/30	1226	1243
121	11/19	1921	1927	167	11/30	1351	1407
122	11/19	2232	2237	168	11/30	1555	1557
123	11/20	107	112	169	11/30	1900	1916
124	11/20	425	429	170	11/30	2222	2228
125	11/20	715	820	171	11/30	2351	37
126	11/20	1123	1124	172	12/ 1	105	109
127	11/20	1138	1205	173	12/ 1	751	806
128	11/20	1333	1353	174	12/ 1	904	955
129	11/20	1616	1657	175	12/ 1	1030	1032
130	11/20	1747	1922	176	12/ 1	1111	1116
131	11/20	2214	2227	177	12/ 1	1312	1334
132	11/21	103	110	178	12/ 1	1614	1625
133	11/21	435	440	179	12/ 1	1913	1936
134	11/21	715	814	180	12/ 1	2002	2003
135	11/21	1120	1156	181	12/ 1	2148	2149
136	11/21	1243	1415	182	12/ 1	2218	2223
137	11/21	1615	1633	183	12/ 1	2351	2352
138	11/21	1739	1746	184	12/ 2	118	122

# THE BDM CORPORATION

TIMES OF PROBABLE RADIO INTERFERENCE DURING SPRSX							
NO.	DATE	TIME START	TIME END	NO.	DATE	TIME START	TIME END
185	12/ 2	749	812	231	12/ 6	1409	1410
186	12/ 2	903	907	232	12/ 6	1616	1710
187	12/ 2	947	948	233	12/ 6	1913	1933
188	12/ 2	1049	1051	234	12/ 6	2221	2229
189	12/ 2	1321	1350	235	12/ 6	2258	2314
190	12/ 2	1535	1529	236	12/ 7	104	112
191	12/ 2	1544	1552	237	12/ 7	429	437
192	12/ 2	1613	1621	238	12/ 7	740	813
193	12/ 2	2211	2215	239	12/ 7	1104	1113
194	12/ 2	2336	2352	240	12/ 7	1315	1410
195	12/ 3	105	112	241	12/ 7	1546	1632
196	12/ 3	139	153	242	12/ 7	1903	1912
197	12/ 3	415	424	243	12/ 7	2213	2213
198	12/ 3	705	717	244	12/ 8	194	202
199	12/ 3	749	813	245	12/ 8	416	427
200	12/ 3	1045	1051	246	12/ 8	712	814
201	12/ 3	1253	1305	247	12/ 8	1014	1018
202	12/ 3	1336	1403	248	12/ 8	1330	1430
203	12/ 3	1705	1745	249	12/ 8	1505	1505
204	12/ 3	2007	2010	250	12/ 8	1612	1650
205	12/ 3	2211	2227	251	12/ 8	1902	1912
206	12/ 3	2346	2347	252	12/ 8	1953	2006
207	12/ 4	33	34	253	12/ 8	2226	2228
208	12/ 4	104	131	254	12/ 9	36	140
209	12/ 4	803	816	255	12/ 9	425	435
210	12/ 4	903	937	256	12/ 9	702	714
211	12/ 4	1110	1114	257	12/ 9	743	813
212	12/ 4	1330	1351	258	12/ 9	1038	1125
213	12/ 4	1507	1521	259	12/ 9	1305	1355
214	12/ 4	1809	1826	260	12/ 9	1600	1629
215	12/ 4	1911	1924	261	12/ 9	1907	1913
216	12/ 4	2230	2256	262	12/ 9	2208	2213
217	12/ 5	422	425	263	12/10	110	117
218	12/ 5	709	813	264	12/10	408	414
219	12/ 5	1144	1217	265	12/10	719	812
220	12/ 5	1425	1439	266	12/10	1103	1117
221	12/ 5	1522	1524	267	12/10	1312	1414
222	12/ 5	1633	1643	268	12/10	1559	1635
223	12/ 5	1735	2009	269	12/10	1925	1959
224	12/ 5	2225	2250	270	12/10	2209	2234
225	12/ 6	105	140	271	12/11	420	447
226	12/ 6	410	417	272	12/11	712	857
227	12/ 6	710	817	273	12/11	1605	1709
228	12/ 6	1003	1029	274	12/11	1923	1926
229	12/ 6	1301	1307	275	12/11	2218	2222
230	12/ 6	1328	1330	276	12/12	440	444

# THE BDM CORPORATION

TIMES OF PROBABLE RADIO INTERFERENCE DURING STREX							
NO.	DATE	TIME START	TIME END	NO.	DATE	TIME START	TIME END
277	12/12	714	804	285	12/13	1227	1310
278	12/12	1054	1120	286	12/13	1613	1644
279	12/12	1314	1443	287	12/13	1911	1916
280	12/12	1636	1656	288	12/13	2211	2219
281	12/12	1921	1932	289	12/14	3	10
282	12/12	2220	2227	290	12/14	57	123
283	12/13	33	111	291	12/14	733	815
284	12/13	429	434				

# THE BDM CORPORATION

## LIST OF FILES AFFECTED BY RADIO INTERFERENCE DURING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF INTERFEFENCE (min)
11/ 5	1	2	1703:36	30
11/ 5	1	3	1735:56	5
11/ 5	1	7	1941:56	16
11/ 5	1	8	2012:36	30
11/ 5	1	9	2044:36	3
11/ 5	1	12	2221:37	9
11/ 6	1	18	135:37	15
11/ 6	1	19	207:57	1
11/ 6	1	25	521:57	14
11/ 6	1	30	803:37	18
11/ 6	1	31	913:37	30
11/ 6	1	32	945:57	2
11/ 7	1	57	559:38	3
11/ 7	1	58	1014:35	4
11/ 7	1	62	1223:55	3
11/ 7	1	66	1435: 1	13
11/ 7	1	71	1821:21	3
11/ 7	1	73	1926: 1	2
11/ 7	1	78	2231: 1	7
11/ 8	1	84	145: 1	9
11/ 8	1	86	249:41	6
11/ 8	1	95	740:41	20
11/ 8	1	96	959: 1	6
11/ 8	1	97	1031:21	1
11/ 8	1	104	1758:42	27
11/ 9	1	126	1349:57	16
11/ 9	1	136	1917:57	4
11/10	1	159	741:37	18
11/10	1	160	813:57	30
11/10	1	161	846:17	4
11/11	1	196	1247:59	15
11/11	1	209	2022:40	15
11/11	1	214	2308:40	2
11/12	1	219	150:20	14
11/12	1	224	432: 0	5
11/12	1	230	746: 1	2
11/12	1	235	1131: 1	2
11/12	2	1	2239: 1	5
11/13	2	6	120:41	5
11/13	2	7	153: 1	2
11/13	2	15	611:41	3
11/13	2	16	644: 1	3
11/13	2	18	748:41	9
11/13	2	28	1626:42	15
11/13	2	29	1659: 2	3



# THE BDM CORPORATION

## LIST OF FILES AFFECTED BY RADIO INTERFERENCE DURING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF INTERFERENCE (min)
11/13	2	35	2233: 2	6
11/14	2	40	114:42	2
11/14	2	41	147: 2	1
11/14	2	46	428:42	3
11/14	2	52	1022:15	3
11/14	2	53	1054:35	2
11/14	2	54	1126:55	1
11/14	2	58	1336:16	13
11/14	2	67	2242:36	5
11/15	2	73	156:36	4
11/15	2	78	438:17	30
11/15	2	80	542:57	3
11/15	2	81	615:17	15
11/15	2	89	1033:57	2
11/15	2	98	1924:56	6
11/15	2	99	1957:16	22
11/16	2	107	101:37	6
11/16	2	108	133:57	27
11/16	2	119	729:37	7
11/16	2	121	1400:58	19
11/16	2	125	1731:38	5
11/16	2	129	1940:58	5
11/16	2	130	2013:18	9
11/16	2	131	2045:38	1
11/16	2	134	2222:38	18
11/16	2	135	2254:58	3
11/17	2	140	136:38	6
11/17	2	146	450:39	2
11/17	2	150	659:59	9
11/17	2	151	732:19	6
11/17	2	154	1357:18	7
11/17	2	159	1943:39	21
11/17	2	160	2015:59	15
11/17	2	164	2225:19	4
11/17	2	165	2257:39	7
11/18	2	170	139:19	6
11/18	2	176	453:18	26
11/18	2	181	734:59	6
11/18	2	182	807:19	3
11/18	2	188	1227:19	2
11/18	2	191	1404:19	10
11/18	2	193	1535:59	7
11/18	2	196	1827:19	2
11/18	2	203	2219: 0	5
11/18	2	204	2251:20	5
11/19	2	207	28:20	17

# THE BDM CORPORATION

## LIST OF FILES AFFECTED BY RADIO INTERFERENCE DURING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF INTERFERENCE (min)
11/19	2	208	100:40	30
11/19	2	209	133: 0	22
11/19	2	210	205:20	3
11/19	2	215	447: 0	6
11/19	2	216	519:20	4
11/19	2	220	728:40	6
11/19	2	222	833:20	10
11/19	2	228	1147:20	7
11/19	2	231	1636:41	22
11/19	2	232	1709: 1	25
11/19	3	5	2256:20	5
11/20	3	10	138: 0	4
11/20	3	16	452: 0	4
11/20	3	21	733:41	19
11/20	3	22	806: 1	30
11/20	3	23	838:21	12
11/20	3	29	1234: 1	1
11/20	3	35	1638: 1	22
11/20	3	36	1936:41	15
11/20	3	41	2218:22	4
11/20	3	42	2250:42	6
11/21	3	47	132:22	7
11/21	3	53	443: 2	5
11/21	3	58	725: 2	10
11/21	3	62	1251:43	9
11/21	3	63	1324: 3	30
11/21	3	64	1356:23	30
11/21	3	65	1428:43	16
11/21	3	69	1638: 3	18
11/21	3	72	1949: 3	8
11/21	3	73	2021:23	1
11/21	3	74	2053:43	9
11/21	3	75	2126: 3	1
11/22	3	82	143: 3	3
11/22	3	91	634: 4	3
11/22	3	93	738:44	4
11/29	3	96	123:20	5
11/29	3	97	155:40	11
11/29	3	99	300:20	10
11/29	3	100	329:20	7
11/29	3	102	434: 0	4
11/29	3	108	748: 0	3
11/29	3	113	1131:20	2
11/29	3	114	1226: 0	3
11/29	3	125	1922:41	10
11/30	3	133	12: 1	8

# THE BDM CORPORATION

## LIST OF FILES AFFECTED BY RADIO INTERFERENCE DURING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF INTERFERENCE (min)
11/30	3	135	116:41	1
11/30	3	136	149: 1	25
11/30	3	141	430:41	11
11/30	3	149	1059: 2	3
11/30	3	153	1556:42	2
12/ 1	3	166	7: 2	16
12/ 1	3	167	37:42	29
12/ 1	3	168	110: 2	4
12/ 1	3	183	2010:22	1
12/ 1	3	187	2219:42	2
12/ 1	3	188	2252: 3	1
12/ 1	3	190	2356:43	1
12/ 2	3	205	1104:23	2
12/ 2	3	214	1939: 4	8
12/ 2	3	219	2220:44	4
12/ 3	3	224	146:44	8
12/ 3	3	225	219: 4	4
12/ 3	3	229	428:24	9
12/ 3	3	234	710: 4	4
12/ 3	4	4	1303:25	5
12/ 3	4	7	2016: 4	3
12/ 3	4	11	2225:24	14
12/ 4	4	14	2:24	1
12/ 4	4	15	34:44	1
12/ 4	4	27	908: 5	5
12/ 4	4	30	1608:45	2
12/ 4	4	33	1915:26	4
12/ 4	4	34	1947:46	6
12/ 5	4	47	441: 5	6
12/ 5	4	54	1550: 6	2
12/ 5	4	57	1758:46	24
12/ 6	4	64	115: 6	10
12/ 6	4	69	442:26	5
12/ 6	4	74	724: 7	14
12/ 6	4	82	1313: 7	6
12/ 6	4	88	1929:47	17
12/ 6	4	89	2002: 7	1
12/ 6	4	94	2240: 8	8
12/ 6	4	95	2312:27	14
12/ 7	4	114	1550:28	4
12/ 7	4	118	1918: 8	4
12/ 7	4	124	2233: 8	5
12/ 8	4	128	117:48	14
12/ 8	4	129	142:49	30
12/ 8	4	130	215: 8	17
12/ 8	4	134	424:29	8

# BDM CORPORATION

## LIST OF FILES AFFECTED BY RADIO INTERFERENCE DURING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF INTERFERENCE (min)
12/ 8	4	149	1510:29	1
12/ 8	4	157	2239:30	2
12/ 9	4	163	425:48	1
12/ 9	4	168	720:28	12
12/ 9	4	169	752:48	10
12/ 9	4	171	1315: 8	10
12/ 9	4	175	1603:29	3
12/ 9	4	180	1934: 9	6
12/ 9	4	185	2215:49	5
12/10	4	199	719:30	1
12/10	4	214	1948:30	23
12/10	4	218	2213:50	5
12/11	4	229	436:31	17
12/11	4	230	502:11	15
12/11	4	235	922:31	4
12/12	5	31	1058:58	5
12/12	5	42	1957:58	4
12/12	5	47	2239:39	7
12/13	5	51	49:58	17
12/13	5	57	431:39	3

# THE BDM CORPORATION

## APPENDIX D

### TIMES OF ANOMALOUS $V_{rms}$

NO.	DATE	TIME START	TIME END	NO.	DATE	TIME START	TIME END
1	11/ 6	1305	1701	47	11/16	15	27
2	11/ 6	1803	2039	48	11/16	137	207
3	11/ 6	2046	121	49	11/16	308	336
4	11/ 7	238	314	50	11/16	431	452
5	11/ 7	354	441	51	11/16	525	601
6	11/ 7	652	946	52	11/16	634	708
7	11/ 7	1126	1131	53	11/16	725	855
8	11/ 7	1304	1309	54	11/16	1122	1514
9	11/ 7	2308	18	55	11/16	1712	2018
10	11/ 8	354	401	56	11/16	2328	2336
11	11/ 8	530	544	57	11/17	108	125
12	11/ 8	1201	1231	58	11/17	252	338
13	11/ 8	1422	1439	59	11/17	926	1228
14	11/ 8	1847	1930	60	11/30	934	939
15	11/ 8	2032	2209	61	12/ 1	547	632
16	11/ 9	414	713	62	12/ 1	709	1413
17	11/ 9	731	933	63	12/ 1	1516	1940
18	11/ 9	1552	1617	64	12/ 1	2033	2100
19	11/ 9	1715	1729	65	12/ 2	355	400
20	11/ 9	2206	2318	66	12/ 2	513	516
21	11/10	45	351	67	12/ 2	608	613
22	11/10	603	823	68	12/ 2	627	714
23	11/10	1202	1559	69	12/ 2	840	951
24	11/10	2130	2342	70	12/ 2	1304	1556
25	11/11	9	108	71	12/ 2	1731	2052
26	11/11	227	626	72	12/ 3	1018	1059
27	11/11	651	656	73	12/ 3	1535	1938
28	11/11	1309	1428	74	12/ 3	2023	2145
29	11/11	1602	1642	75	12/ 4	247	335
30	11/11	1740	1820	76	12/ 4	528	553
31	11/11	2259	256	77	12/ 4	714	820
32	11/12	610	810	78	12/ 4	900	1007
33	11/12	1154	1207	79	12/ 4	1106	1151
34	11/12	1419	1427	80	12/ 4	1339	1406
35	11/12	1539	1636	81	12/ 4	1507	1557
36	11/12	2050	2311	82	12/ 4	1913	1954
37	11/13	29	58	83	12/ 4	2024	2030
38	11/13	224	614	84	12/ 4	2322	2356
39	11/13	704	839	85	12/ 5	110	152
40	11/13	1007	1234	86	12/ 5	315	338
41	11/13	1606	1620	87	12/ 5	654	729
42	11/13	2045	2338	88	12/ 5	752	921
43	11/14	627	830	89	12/ 5	1122	1217
44	11/14	935	1800	90	12/ 5	1238	1245
45	11/15	1452	1745	91	12/ 5	1310	1313
46	11/15	2216	2320	92	12/ 5	1521	1556

# THE BDM CORPORATION

## TIMES OF ANOMALOUS Vrms (EXCLUDING RFI) DURING STREX

NO.	DATE	TIME START	TIME END	NO.	DATE	TIME START	TIME END
93	12/ 5	1633	2005	115	12/ 8	1908	2008
94	12/ 5	2048	2138	116	12/ 8	2318	2359
95	12/ 5	2226	146	117	12/ 9	300	440
96	12/ 6	307	337	118	12/ 9	702	815
97	12/ 6	551	555	119	12/ 9	1308	1445
98	12/ 6	710	835	120	12/ 9	1948	2004
99	12/ 6	941	1033	121	12/ 9	2327	10
100	12/ 6	1451	1718	122	12/10	305	344
101	12/ 6	1919	1954	123	12/10	404	412
102	12/ 6	2040	2055	124	12/10	1109	1205
103	12/ 6	2221	2349	125	12/10	1509	1554
104	12/ 7	300	354	126	12/10	1917	2002
105	12/ 7	721	815	127	12/10	2318	4
106	12/ 7	1052	1144	128	12/11	411	723
107	12/ 7	1503	1634	129	12/11	1827	1854
108	12/ 7	1736	1740	130	12/12	905	928
109	12/ 7	1948	2001	131	12/13	731	817
110	12/ 7	2316	2349	132	12/13	1057	1101
111	12/ 8	302	350	133	12/13	1117	1128
112	12/ 8	710	816	134	12/14	340	424
113	12/ 8	1052	1207	135	12/14	652	656
114	12/ 8	1500	1549				

# THE BDM CORPORATION

FILES WITH ANOMALOUS  $V_{rms}$  FOR RELATIVE WINDS WITHIN 60 DEGREES  
OF BOW DURING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF EVENT (min)	<RDir>
11/ 6	1	37	1308:17	3	337
11/ 6	1	41	1920:38	30	316
11/ 6	1	42	1952:58	30	318
11/ 6	1	43	2025:18	30	314
11/ 6	1	44	2057:38	23	318
11/ 6	1	47	2234:38	30	22
11/ 6	1	48	2306:58	30	317
11/ 6	1	49	2339:38	30	313
11/ 7	1	50	11:58	30	331
11/ 7	1	52	116:38	30	53
11/ 7	1	53	148:58	2	32
11/ 7	1	55	253:58	16	331
11/ 7	1	56	326:13	13	332
11/ 7	1	58	1014:35	1	355
11/ 7	1	61	1151:35	5	355
11/ 7	1	64	1328:35	5	354
11/ 8	1	82	40:21	8	355
11/ 8	1	91	531:21	1	11
11/ 9	1	122	1002: 3	1	353
11/ 9	1	130	1559:17	7	29
11/ 9	1	131	1631:37	15	325
11/ 9	1	133	1740:57	14	6
11/10	1	147	113:37	29	324
11/10	1	148	145:57	30	334
11/10	1	149	218:17	30	334
11/10	1	150	250:37	30	326
11/10	1	151	322:57	30	323
11/10	1	152	355:17	26	337
11/10	1	156	604:37	2	5
11/10	1	160	813:57	30	320
11/10	1	161	846:17	7	34
11/10	1	165	1403:18	30	341
11/10	1	166	1435:38	30	313
11/10	1	176	2335:38	30	9
11/11	1	177	7:58	4	13
11/11	1	184	354:18	30	357
11/11	1	185	426:39	30	341
11/11	1	186	458:59	30	310
11/11	1	187	531:19	30	323
11/11	1	188	603:39	30	343
11/11	1	199	635:59	20	349
11/11	1	190	708:19	5	1
11/11	1	197	1320:19	11	8
11/11	1	198	1352:39	30	350
11/11	1	199	1424:59	30	349
11/11	1	201	1603:59	2	20

# THE BDM CORPORATION

FILES WITH ANOMALOUS Vrms FOR RELATIVE WINDS WITHIN  
60 DEGREES OF BOW DURING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF EVENT (min)	<FDir>
11/11	1	202	1636:19	30	57
11/11	1	203	1708:39	3	4
11/11	1	204	1740:59	1	14
11/11	1	206	1845:39	4	59
11/11	1	214	2308:40	10	347
11/12	1	218	118: 0	30	313
11/12	1	219	150:20	30	301
11/12	1	220	222:40	30	309
11/12	1	221	255: 0	30	320
11/12	1	228	641:20	30	346
11/12	1	229	713:41	30	321
11/12	1	230	746: 1	30	310
11/12	1	238	1610:41	30	353
11/12	1	239	1643: 1	23	317
11/12	1	245	2051:21	1	8
11/13	2	5	120:41	7	24
11/13	2	8	225:21	1	15
11/13	2	9	257:41	30	334
11/13	2	10	330: 1	30	308
11/13	2	11	402:21	30	308
11/13	2	14	539:21	30	323
11/13	2	17	716:21	12	36
11/13	2	20	1037:21	30	335
11/13	2	21	1109:41	30	335
11/13	2	22	1142: 1	30	331
11/13	2	23	1214:21	30	337
11/13	2	28	1626:42	14	3
11/13	2	34	2200:42	30	324
11/13	2	35	2233: 2	30	316
11/13	2	36	2305:22	30	316
11/13	2	37	2337:42	30	310
11/14	2	56	1231:35	30	306
11/14	2	57	1303:55	30	311
11/14	2	58	1336:16	30	338
11/14	2	59	1448:36	30	352
11/14	2	60	1520:56	30	347
11/14	2	61	1603:56	30	354
11/15	2	93	1505:38	14	324
11/15	2	95	1604:18	30	326
11/15	2	104	2324:37	25	26
11/16	2	106	29:17	12	44
11/16	2	109	206:17	29	302
11/16	2	111	310:57	3	54
11/16	2	112	343:17	23	333
11/16	2	114	447:57	17	330
11/16	2	115	520:17	2	30
11/16	2	117	624:57	6	29



# THE BDM CORPORATION

FILES WITH ANOMALOUS Vrms FOR RELATIVE WINDS WITHIN  
60 DEGREES OF BOW DUPING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF EVENT (min)	<RDir>
11/16	2	119	729:37	13	360
11/16	2	125	1731:38	20	325
11/16	2	126	1803:58	30	308
11/16	2	127	1836:18	30	313
11/16	2	129	1940:58	30	338
11/17	2	143	313:38	22	330
11/17	2	144	345:58	22	320
12/ 1	3	177	601: 3	14	351
12/ 1	3	178	633:23	29	336
12/ 1	3	181	902:43	30	315
12/ 1	3	184	2042:42	10	20
12/ 1	3	185	2115: 2	15	351
12/ 2	3	197	414:43	5	6
12/ 2	3	199	519:23	3	3
12/ 2	3	201	624: 3	5	4
12/ 2	3	202	743: 3	1	13
12/ 2	3	203	843:43	4	352
12/ 2	3	209	1313:43	10	322
12/ 2	3	216	2043:44	30	306
12/ 2	3	217	2116: 4	6	359
12/ 3	3	239	1023:45	6	352
12/ 3	4	1	1126:45	2	359
12/ 3	4	6	1943:45	24	325
12/ 3	4	8	2048:24	25	325
12/ 3	4	9	2120:44	30	4
12/ 3	4	10	2153: 4	22	16
12/ 4	4	18	305:25	13	331
12/ 4	4	19	337:45	27	319
12/ 4	4	23	547: 5	19	351
12/ 4	4	24	619:25	4	11
12/ 4	4	26	724: 5	10	321
12/ 4	4	27	908: 5	8	348
12/ 4	4	29	1536:25	29	307
12/ 4	4	30	1608:45	18	344
12/ 4	4	33	1915:26	2	355
12/ 4	4	35	2020: 6	4	11
12/ 4	4	38	2323: 5	6	356
12/ 5	4	43	210:45	11	345
12/ 5	4	53	1123:46	2	6
12/ 5	4	54	1550: 6	29	304
12/ 5	4	55	1622:26	4	13
12/ 5	4	56	1726:25	30	351
12/ 5	4	57	1758:46	30	355
12/ 6	4	64	115: 6	30	2
12/ 6	4	65	213:26	3	33
12/ 6	4	68	403:46	3	18
12/ 6	4	72	619:27	4	10

# THE BDM CORPORATION

FILES WITH ANOMALOUS  $V_{rms}$  FOR RELATIVE WINDS WITHIN  
60 DEGREES OF  $\beta_{OW}$  DURING STREX

DATE	TAPE NO.	FILE NO.	TIME AT END OF FILE	DURATION OF EVENT	(min)	<RDir>
12/ 6	4	74	724: 7	14		332
12/ 6	4	75	852: 7	13		6
12/ 6	4	77	956:47	16		331
12/ 6	4	78	1102:27	1		2
12/ 6	4	84	1612: 7	30		314
12/ 6	4	88	1929:47	11		11
12/ 6	4	89	2002: 7	22		341
12/ 6	4	91	2106:47	15		319
12/ 6	4	94	2240: 8	19		10
12/ 6	4	95	2312:27	30		9
12/ 7	4	110	1054: 7	2		2
12/ 7	4	115	1741: 8	4		353
12/ 7	4	120	2022:48	6		359
12/ 8	4	143	1056:49	5		15
12/ 8	4	144	1140:49	30		316
12/ 8	4	145	1213: 9	24		311
12/ 8	4	149	1510:29	10		325
12/ 9	4	160	16:30	12		328
12/ 9	4	163	425:48	30		10
12/ 9	4	171	1315: 8	7		5
12/ 9	4	172	1426:48	30		10
12/ 9	4	181	2006:29	16		349
12/10	4	189	25: 9	15		336
12/10	4	193	335: 9	30		8
12/10	4	194	407:29	10		43
12/11	4	229	436:31	26		304
12/11	5	5	1845:57	19		339
12/11	5	6	1918:17	6		50
12/12	5	28	921:58	17		13
12/12	5	29	954:18	4		22
12/13	5	67	1103:59	4		352

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## REFERENCES

1. "Naval Postgraduate School Shipboard and Aircraft Meteorological Equipment," G. E. Schacher, K. L. Davidson, D. E. Spiel and C. W. Fairall, Technical Report, NPS-61-80-017 (1980).
2. "Observation of the Temperature Structure Function Parameter,  $C_T^2$ , Over the Ocean," K. L. Davidson, T. M. Houlihan, C. W. Fairall and G. E. Schacher, Boundary-Layer Meteorology, 15, 507-523 (1978).
3. "Measurements of the Humidity Structure Function Parameters,  $C_q^2$  and  $C_{Tq}$ , Over the Ocean," C. W. Fairall, G. E. Schacher and K. L. Davidson, Boundary-Layer Meteorology, 19, 81-92 (1980).
4. "An Aircraft Study of Turbulence Dissipation Rate and Temperature Structure Function in the Unstable Marine Atmospheric Boundary Layer," C. W. Fairall, Ralph Markson, G. E. Schacher and K. L. Davidson, Boundary-Layer Meteorology, 19, 453-469 (1980).

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